

DE LA RECHERCHE À L'INDUSTRIE

cea den

# From fuel to fuel: Dissolution, Partitioning and fuel manufacturing

## ASGARD, SACSESS, GENIORS

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Christian Ekberg





**TURNING  
SPENT NUCLEAR FUEL  
INTO A RESOURCE**

**INTRODUCTION  
THE 3 PROJECTS  
EDUCATION AND TRAINING**



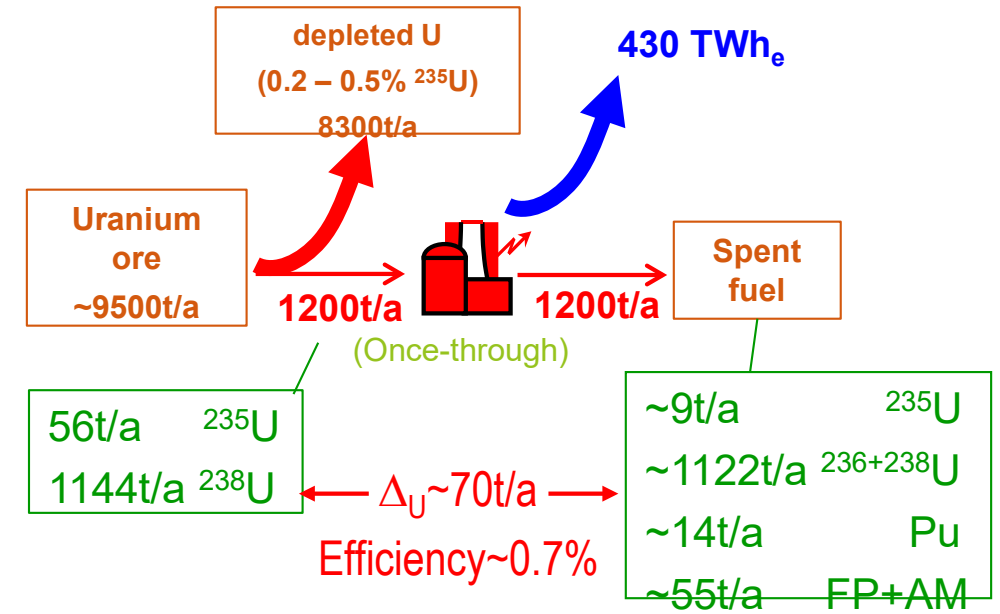
**TURNING  
SPENT NUCLEAR FUEL  
INTO A RESOURCE**

## INTRODUCTION

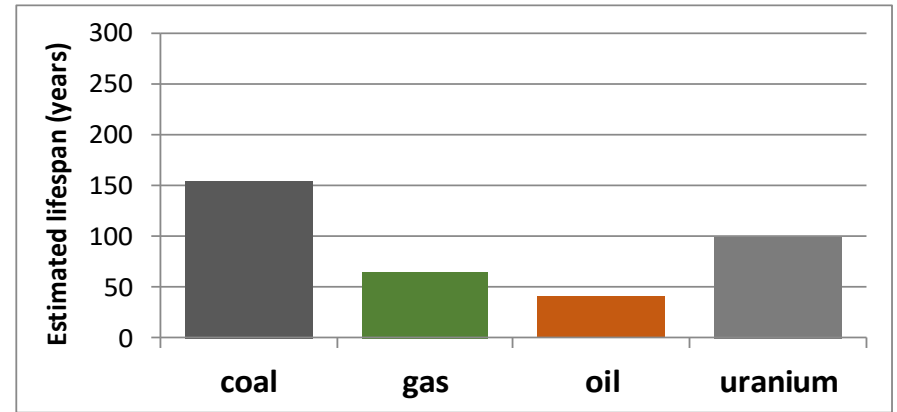


Does not preserve natural resource

- **Natural U is a limited resource**
  - Although present everywhere, U-ores of reasonable economic interest are limited (260\$/kg U)
  - Minimum lifespan ~135 years (with current consumption 56kt/y)
  - Need for preserving U-resource
  
- **Global efficiency is currently very low: ~0.7%**
  - ~70t from the initial ~9500t Uore
  
- **Need for improving U-efficiency**

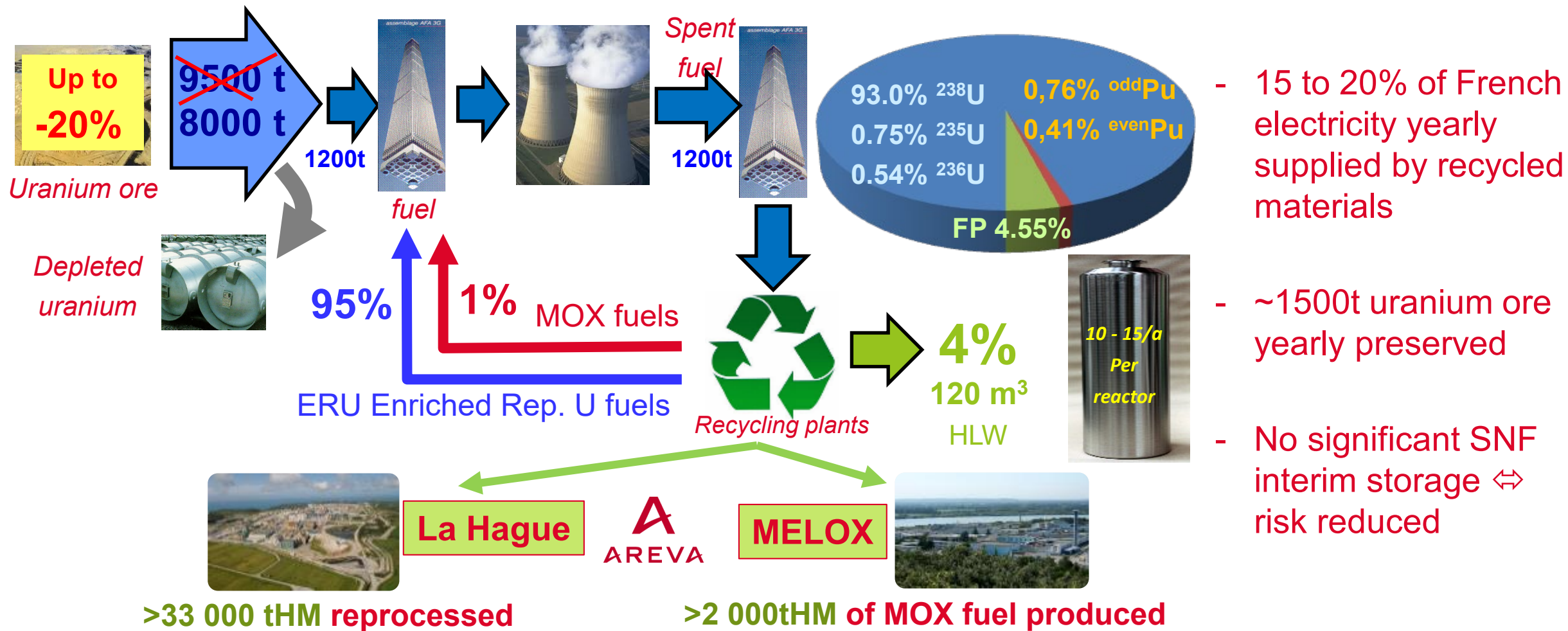


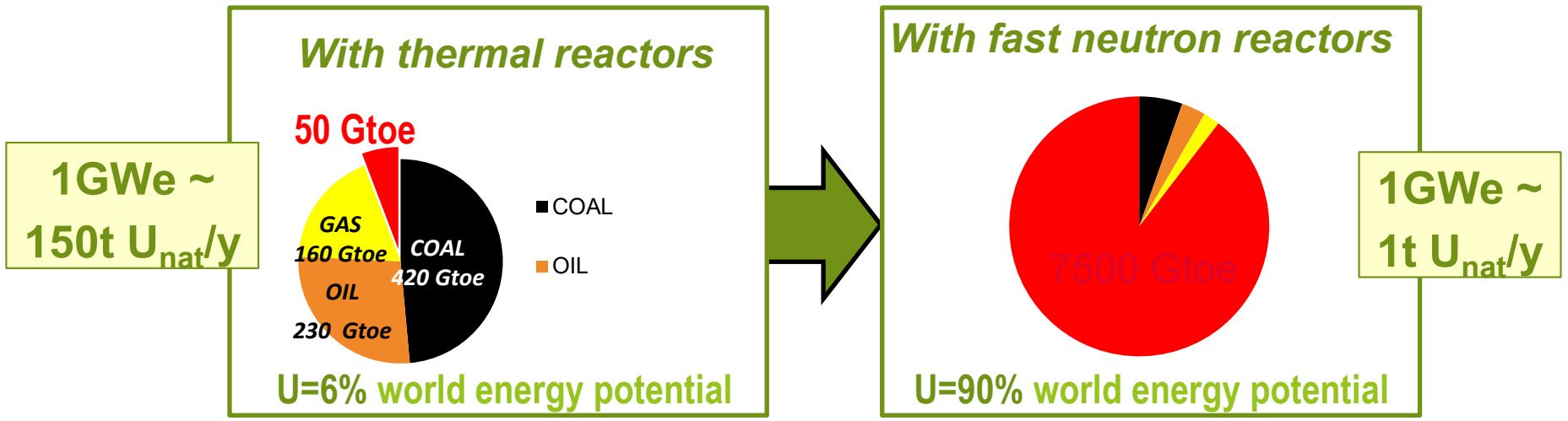
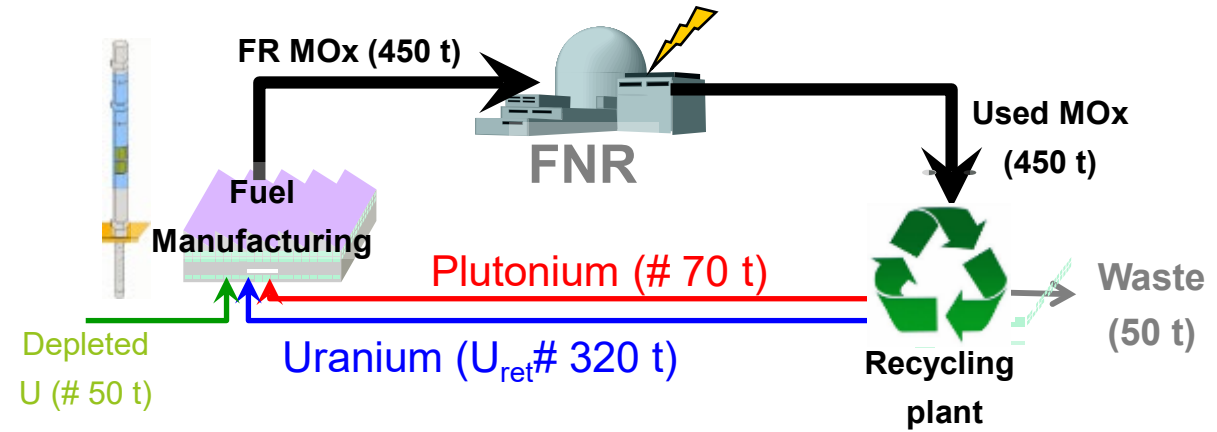
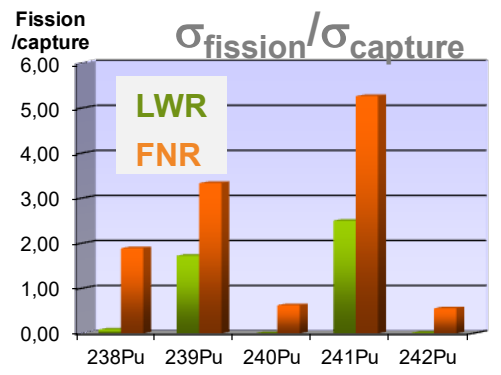
Rough estimates derived from French Fuel cycle assuming no recycling



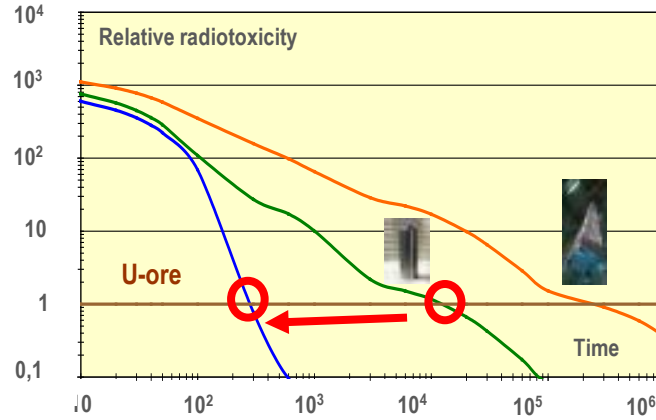
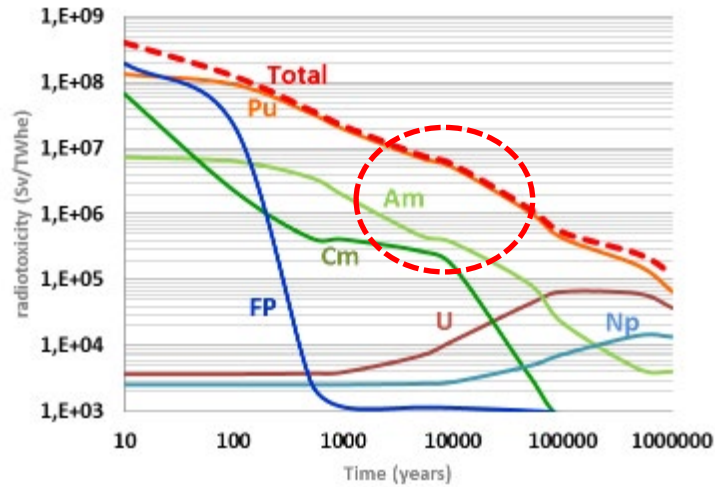


# Nuclear Energy Today – Once through fuel cycle (French fuel cycle)





**Very significant improvement of natural uranium efficiency**



➤ Waste toxicity dominated by MA

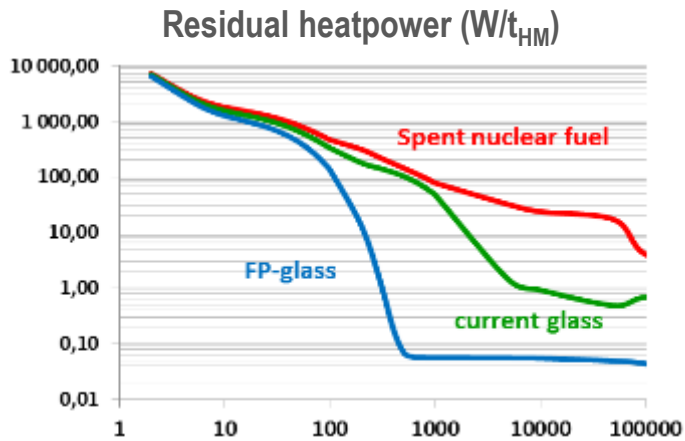
■ Recycling MA ⇔ decrease waste lifetime and toxicity

➤ Preserve the valuable repository resource

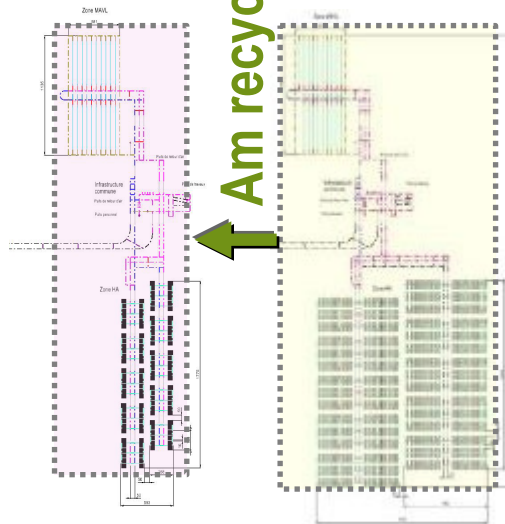
■ ↓ of the heat load ⇔ ↑ density of the repository

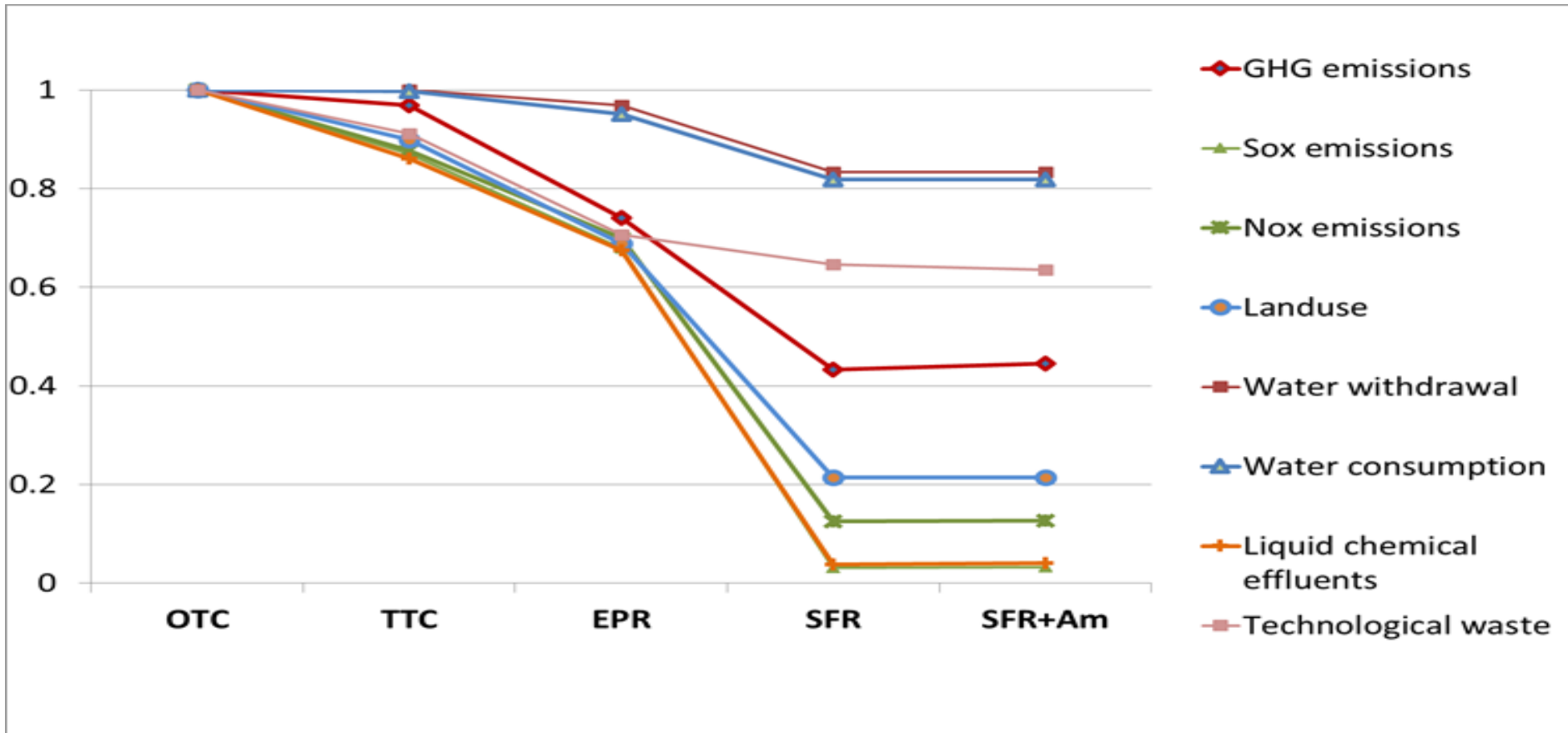
■ With Am recycling, reduction of the repository volume by a factor up to 8

■ Very significant increase of the repository "lifespan"



HLW: 160 ha      HLW: 1200 ha

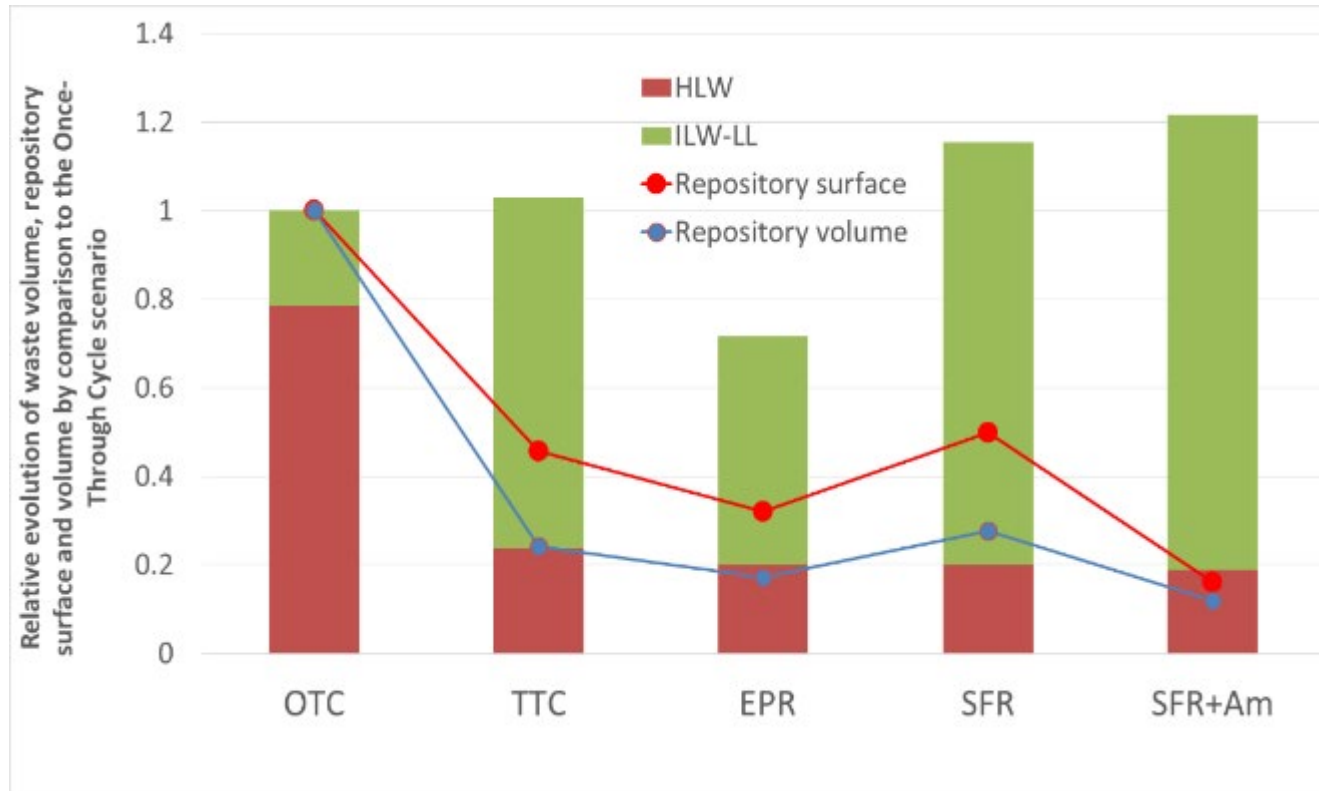




Actinides recycling significantly improve the nuclear energy environmental footprint

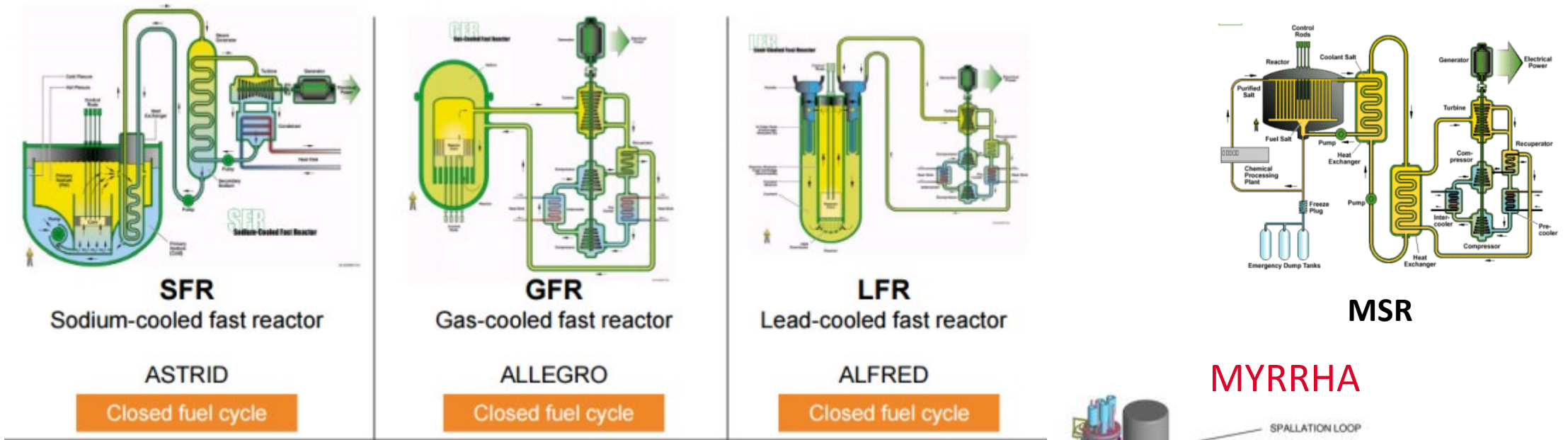
Ch. Poinssot, S. Bourg et al., Energy 2014, 6, 199–211  
J.Serp, Ch Poinssot, S. Bourg, Energies 2017, 10, 1445.





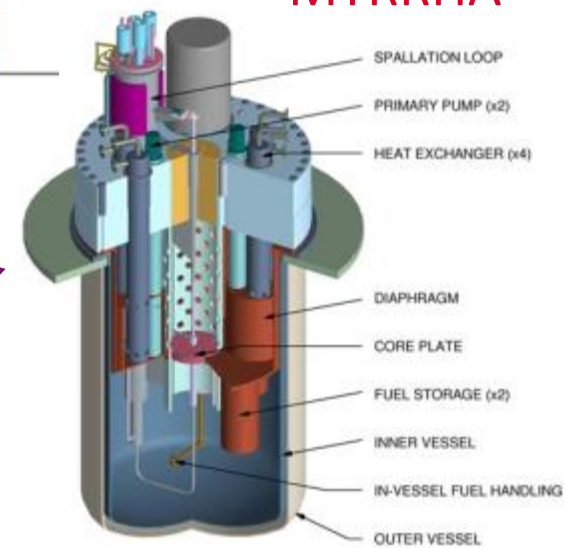
Interim storage time:  
120 years

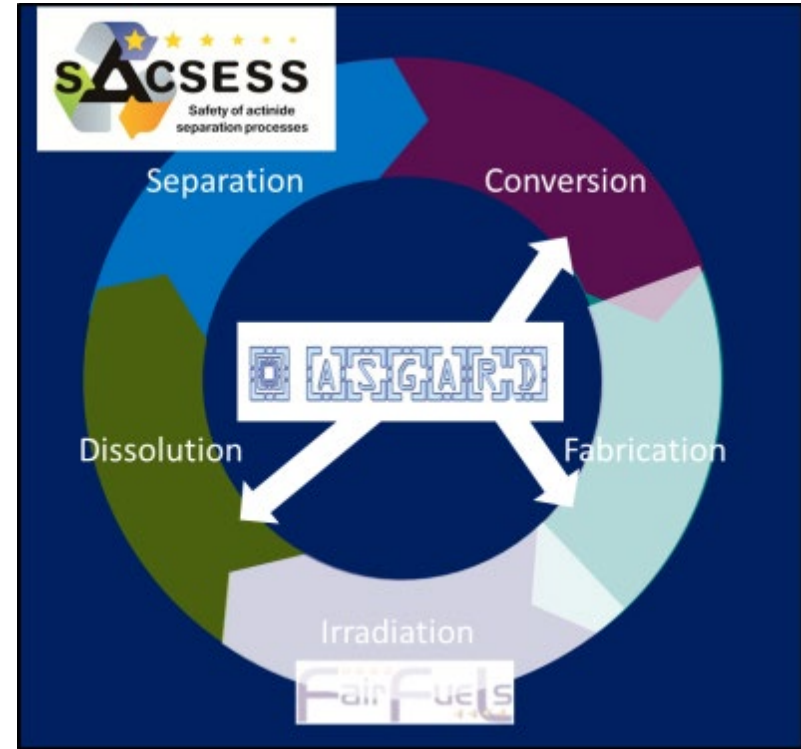
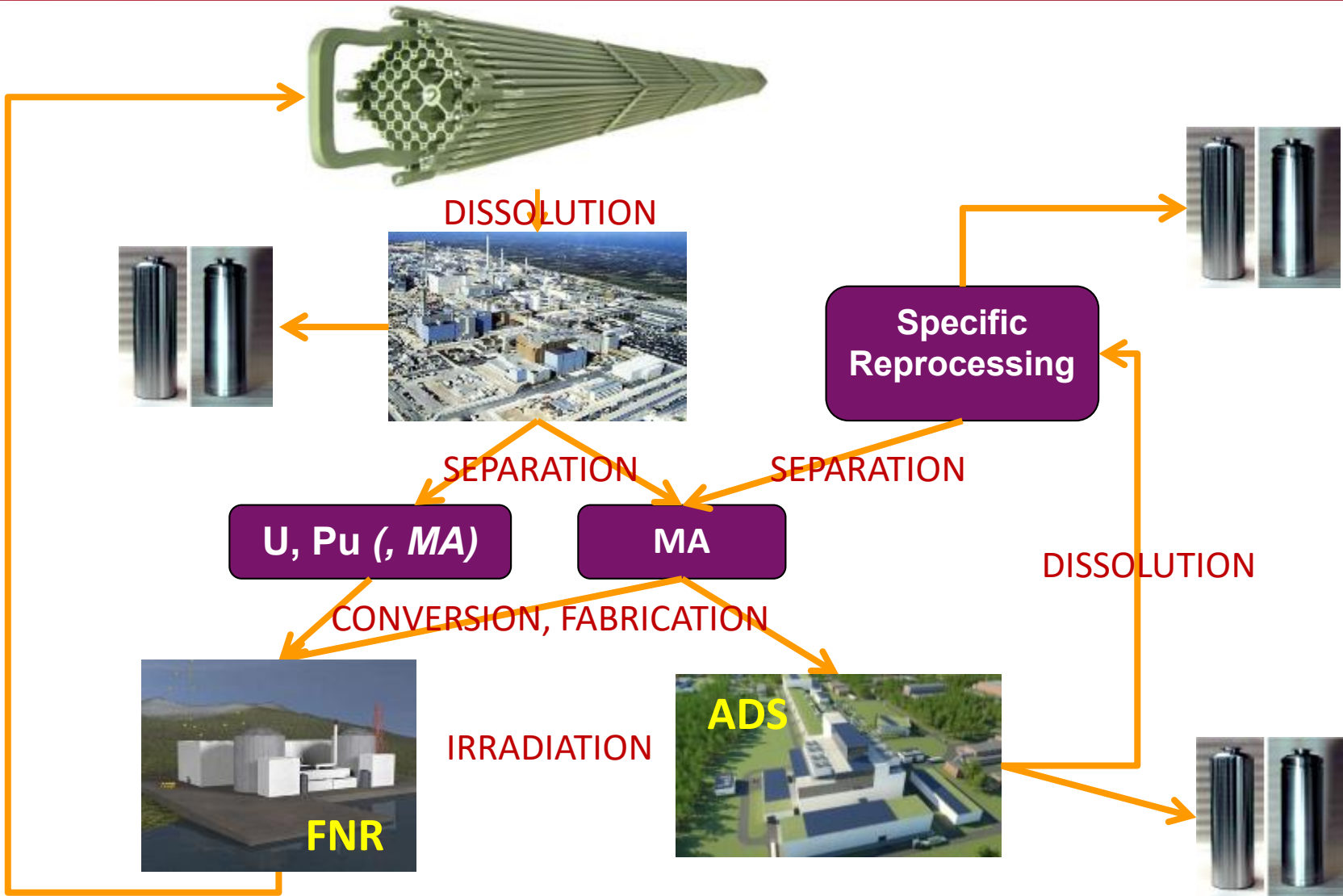
- Relative decrease of HLW vs. ILW while total volume of waste ~ constant +/- 20%
- Decrease of thermal power due to Pu-recycling → significant gain for the repository volume
- Decrease of radiotoxicity & lifetime
- Am transmutation: save the repository surface by a factor about 3 compared to SFR



Reference fuel: carbide, nitride...

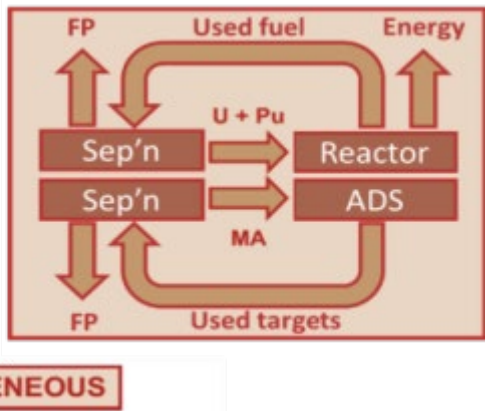
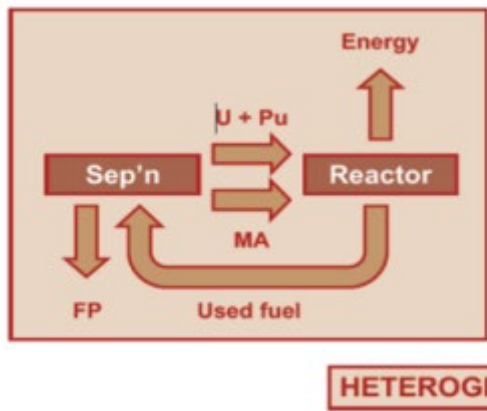
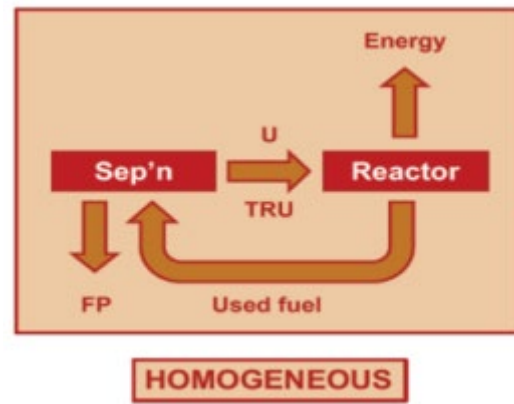
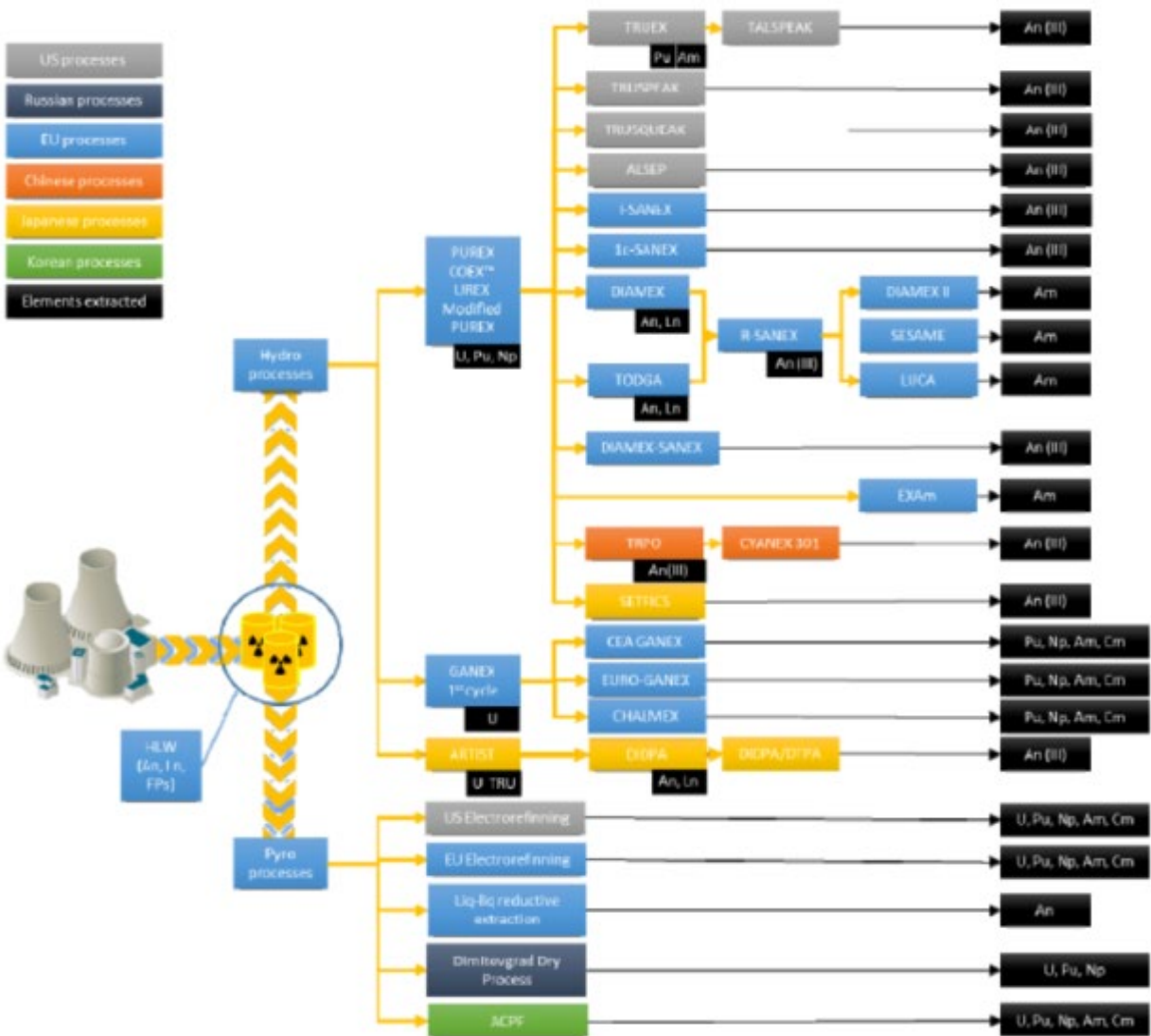
Reference fuel: MOX







# Different separation process options developed worldwide for different fuel cycle strategies



But before, we need to dissolve the fuel, and after, we have to re-manufacture it!



**TURNING  
SPENT NUCLEAR FUEL  
INTO A RESOURCE**

**ASGARD**

**FROM FUEL TO FUEL**

**NON MOX**





ASGLARD



**Christian Ekberg, Stephane Bourg, Eva deVisser-Tynova, Andreas Geist, Frodo Klaassen,  
Teodora Retegan, Mark Sarsfield and Janne Wallenius**

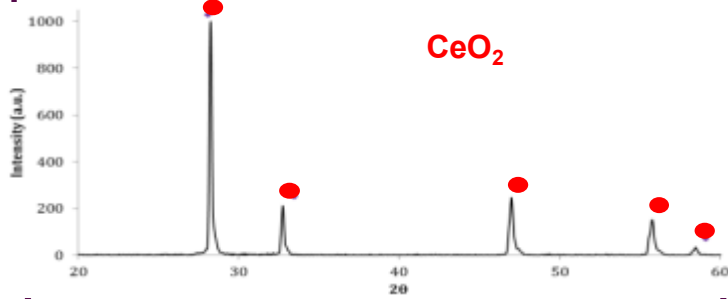
- Budget: 9365 kEuro (EC 4.9 kEuro)
- Duration: 20120101- 20151231  
(4 years)
- Extended to 20150630



- Focus on the behaviour of novel nuclear fuels ranging through production, dissolution, conversion and refabrication
- Novel fuels considered are An (Am) bearing oxides, CERMET (Mo-based), CERCER (Mg based)', nitrides and carbides
- Provide extensive training and education concerning handling of nuclear material from the whole fuel

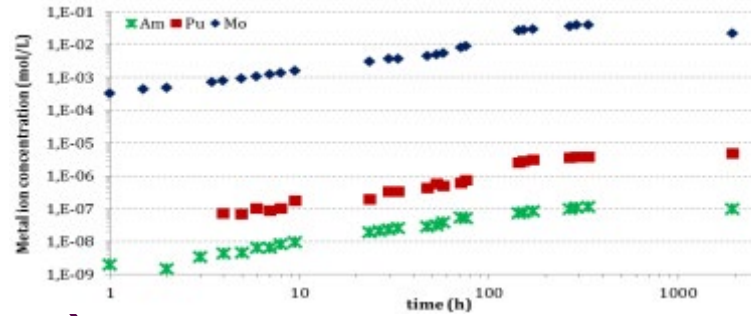
## CeO<sub>2</sub>/Mo dissolution

- CeO<sub>2</sub> /Mo (60/40wt.%) pellets dissolved in 20 and 100 mL 1 mol/L HNO<sub>3</sub> without or with Fe(III)
- CeO<sub>2</sub> separated from the matrix



## PuO<sub>2</sub>/Mo dissolution

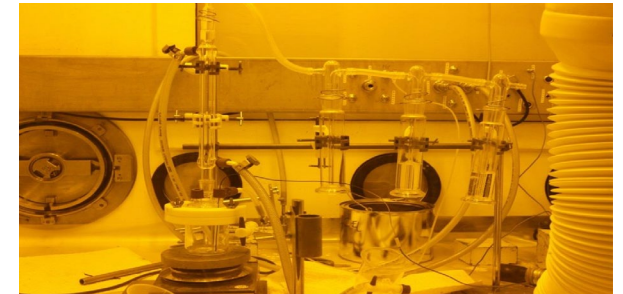
- 1 and 3 mol/L HNO<sub>3</sub> and 1 mol/L HNO<sub>3</sub>/0.2 mol/L Fe(NO<sub>3</sub>)<sub>3</sub>, RT
- Mo dissolution – faster with Fe (III)
- Pu (Am) dissolution much slower in presence of Fe(III)
- PuO<sub>2</sub> could be separated from Mo matrix



Fresh fuel

## (Pu<sub>0.8</sub>Am<sub>0.2</sub>)O<sub>2</sub>/ Mo dissolution

- Irradiated at HFR Petten (HELIOS pin 5)
- 2 steps process:
  - dissolution of Mo -matrix HNO<sub>3</sub> (8 M)
  - dissolution of actinides oxides HF or Ag(II)
- ❑ Samples taken during dissolution for ICP measurements
- ❑ Black residue remained – PuO<sub>2</sub>



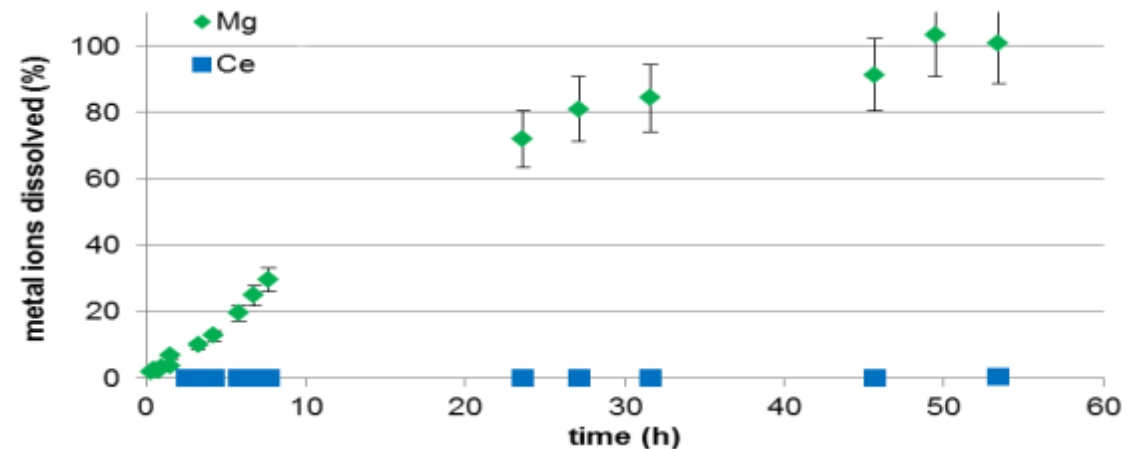
Irradiated fuel



- Experiments in 2.5 mol/L HNO<sub>3</sub> at 30 °C.
- Agitation speed has no effect on dissolution rate, i.e. **dissolution rate is surface controlled**
- The acid volume has no effect on dissolution rate.
- A two-stage reaction equation for the dissolution of MgO was postulated based on XRD measurements and literature review.
- The dissolution (2 M HNO<sub>3</sub>, RT) of MgO/CeO<sub>2</sub> (60/40 wt.%) – MgO completely dissolved, CeO<sub>2</sub> remained as powder



- **Actinides can be separated from the magnesia matrix**

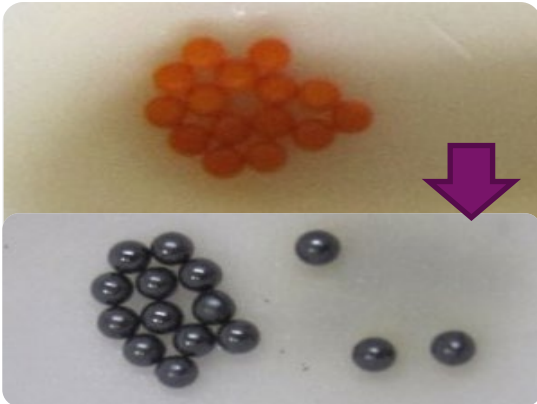




## Sol – gel methods

### Two methods

- *Internal gelation*
- *Complex Sol-Gel Process*
- UO<sub>2</sub>/Nd microspheres prepared & characterized
- processes studied & optimised



## Impregnation of solid matrixes

- Amberlite IRC-86 and Lewatit TP-207 resins tested for fabrication of UO<sub>2</sub>/Nd microspheres
- Amberlite IRC-86 successful

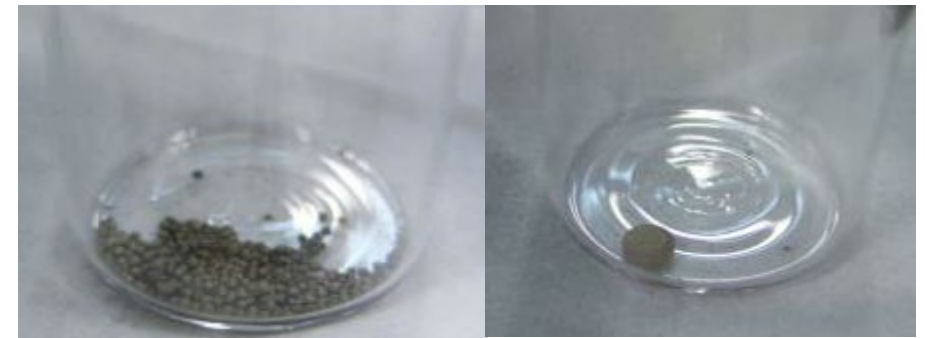
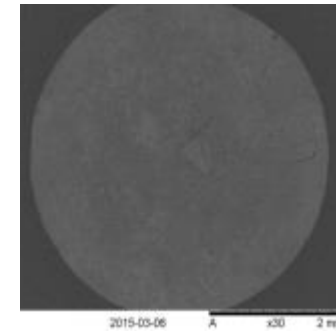


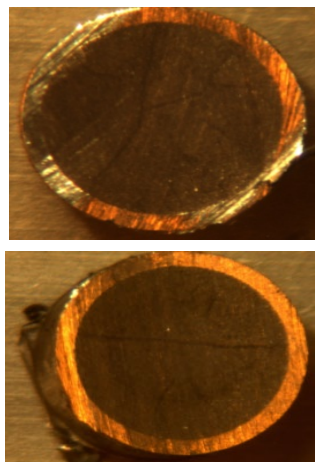
## Photochemical conversion

- UO<sub>2</sub>, ThO<sub>2</sub>, ThO<sub>2</sub>-UO<sub>2</sub>, CeO<sub>2</sub>, Eu<sub>2</sub>O<sub>3</sub>, (Ce,U)O<sub>2</sub>, Eu<sub>2</sub>O<sub>3</sub>-UO<sub>2</sub> materials prepared
- Fuel pellets made



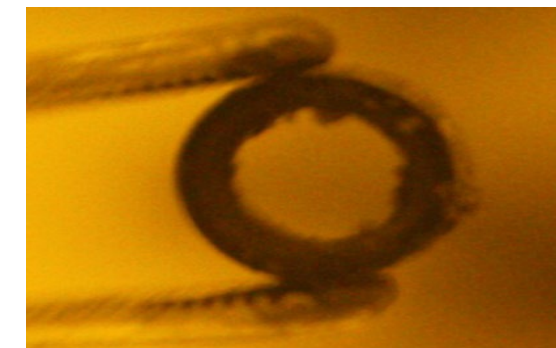
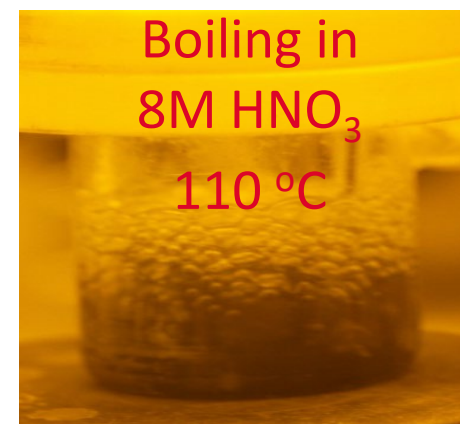
- Sol-gel beads and pellets of ZrN and (Pu,Zr)N has been manufactured
  - EXAFS show one structure for (Pu, Zr)N
- (Pu,Zr)N pellets sintered in Ar or N<sub>2</sub>
  - The ones in N<sub>2</sub> has two crystal structures
  - The ones in Ar has one crystal structure
- Problems with carbon content but being solved
- The expected blackberry structure could be avoided and a smooth pellet achieved





CONFIRM pin slices  
(including cladding)

- $m \approx 1.13 - 1.27 \text{ g}$
- $h \approx 4.6 - 5.2 \text{ mm}$
- $\text{Pu} \approx 400 - 440 \text{ mg}$

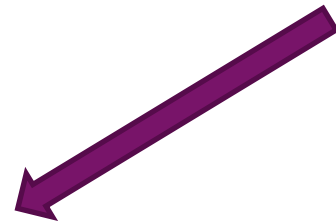
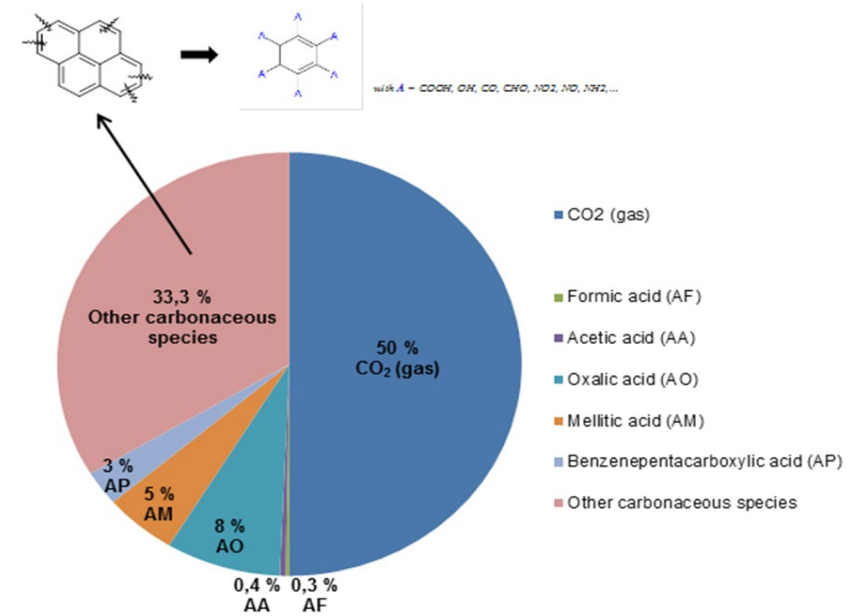
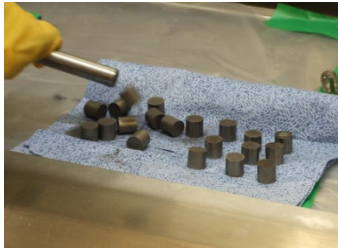


*Exp. 1*

	Exp. 1	Exp. 2	Exp. 3	Exp. 4
<b>Additions</b>	-	1 M HF*	0.8 M HF	250 mg AgO
<b>Boiling time (h)</b>	13	23	6	16
<b>Liquid volume (ml)</b>	100	100	150	100
<b>Undissolved fuel on cladding</b>	YES	<b>NO</b> (or little)	<b>NO</b>	YES
<b>Solid residue (particles) (Zr cont.)</b>	YES	YES	<b>NO</b>	YES
<b>Remaining solid (clad.+fuel) (mg)</b>	547	574	117	716

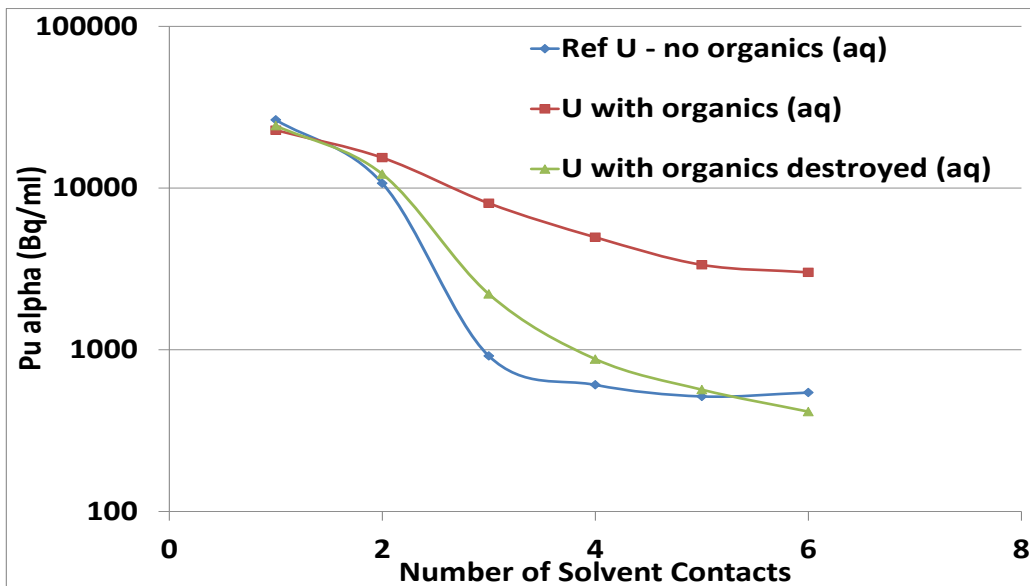
- Pin starts to dissolve from the middle
- HF necessary for complete dissolution

\* added after 54h



“Uranium carbide dissolution in nitric acid: organic compounds speciation”  
S. Legand, C. Bouyer, F. Casanova, D. Lebeau and C. Lamouroux (submitted).

“Dissolution of Uranium Carbide Fuel pellets” M.J. Sarsfield, C.J. Maher, T.L. Griffiths (submitted).







**TURNING  
SPENT NUCLEAR FUEL  
INTO A RESOURCE**

**SACSESS**

**IMPROVING THE SAFETY OF SPENT FUEL  
REPROCESSING**





## SACSESS, 2013-2016

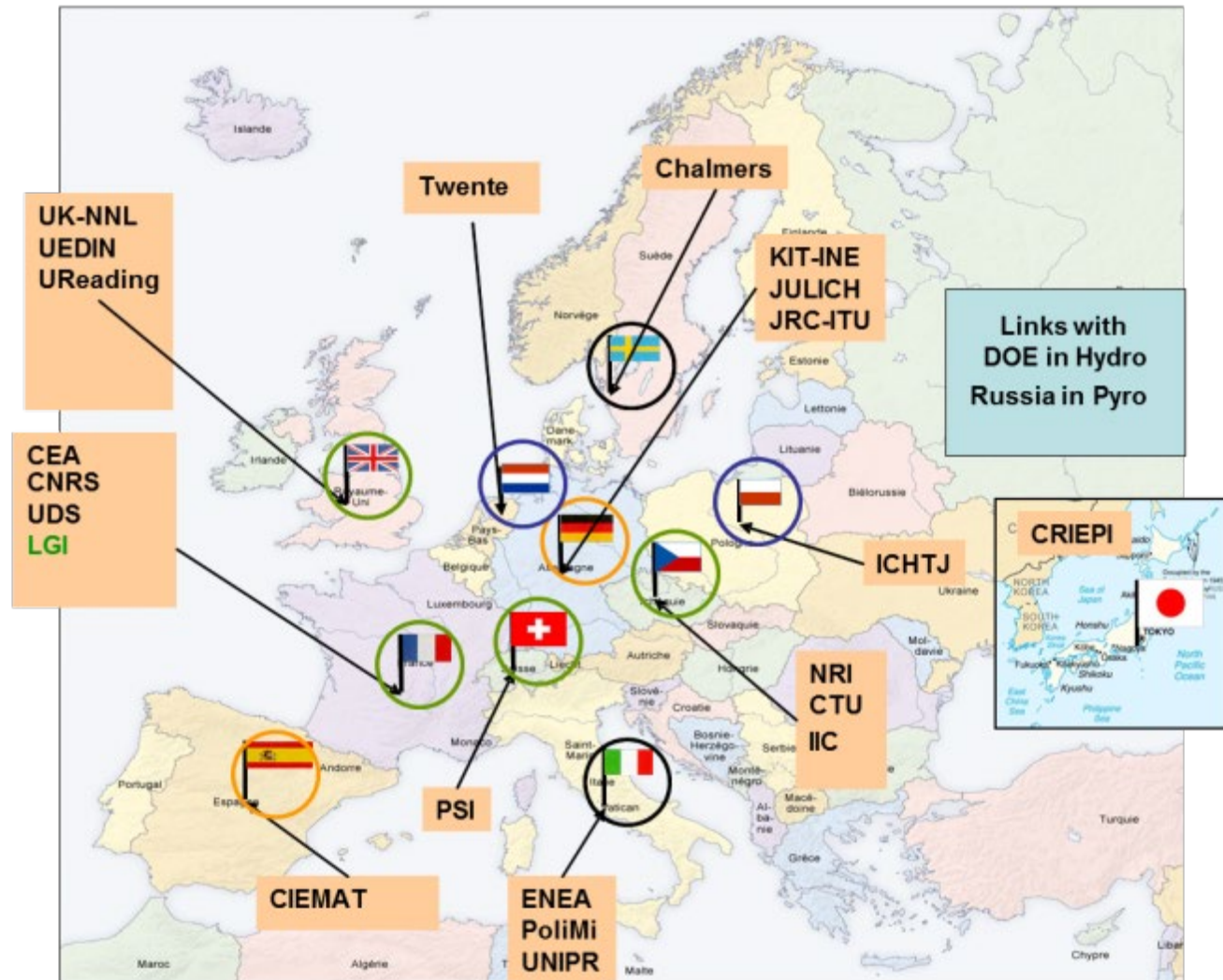
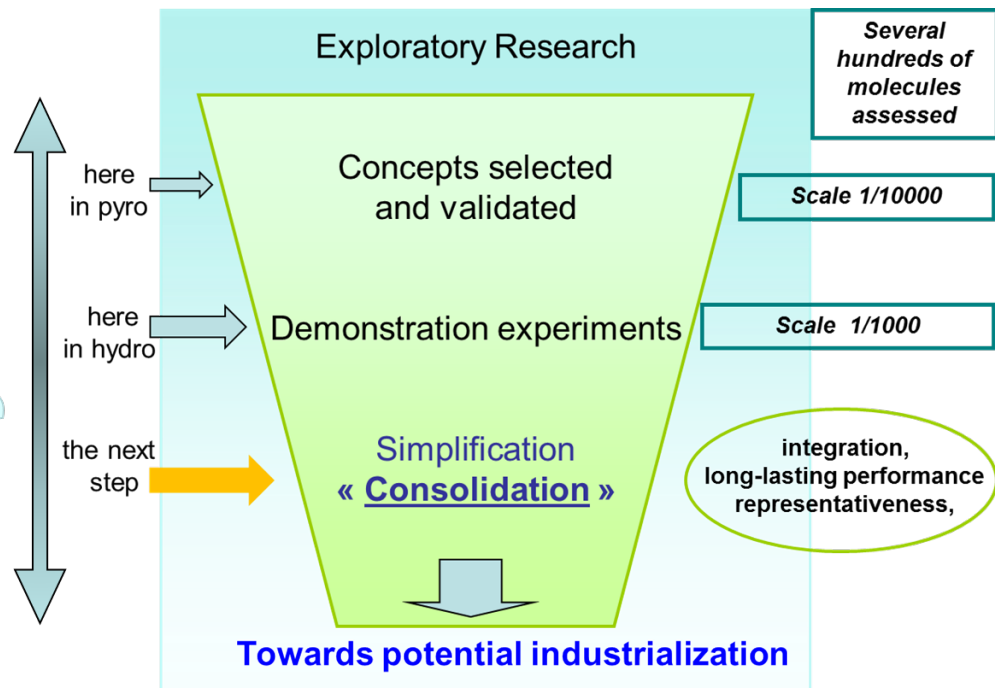
26 Partners

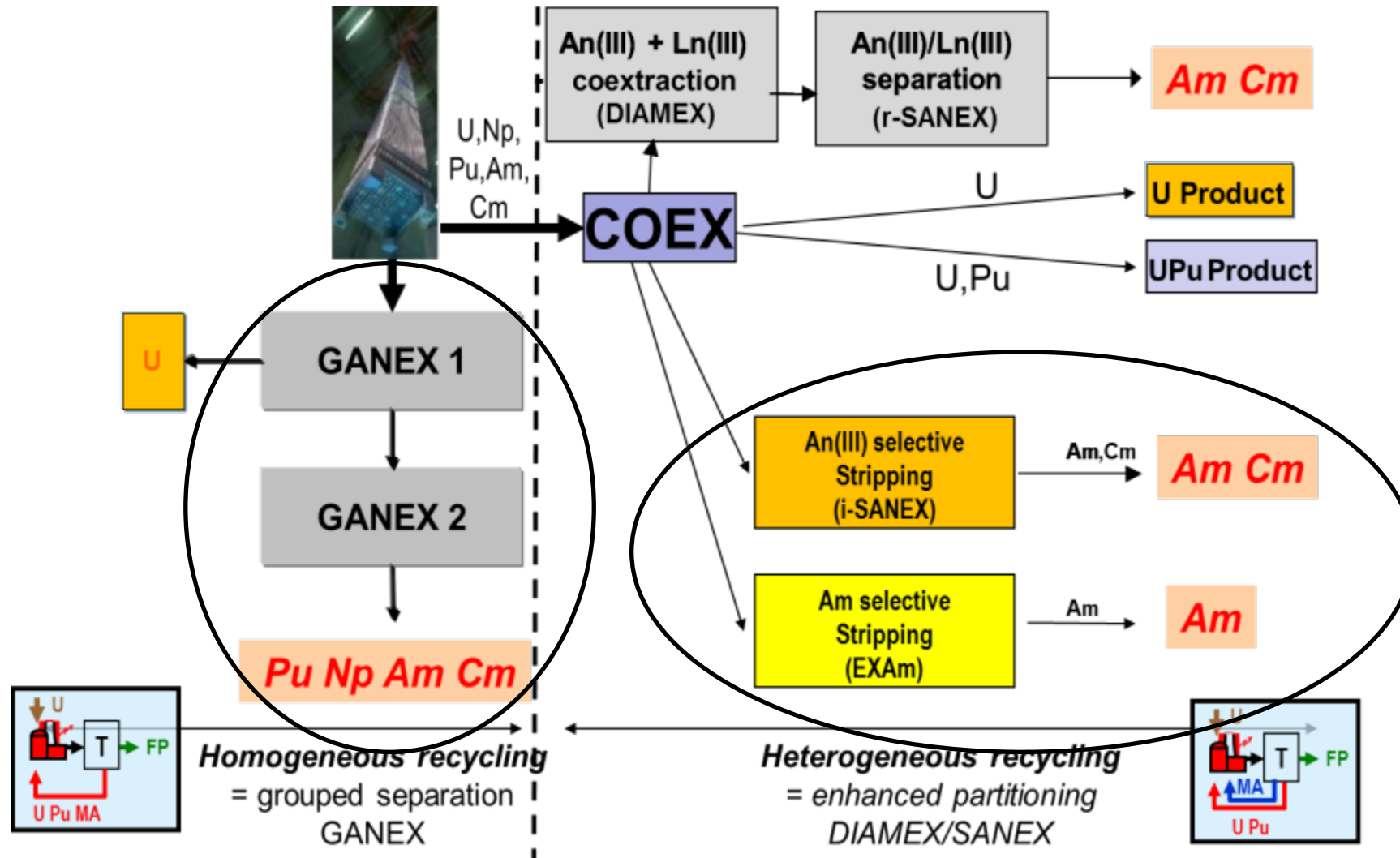
2013-2015

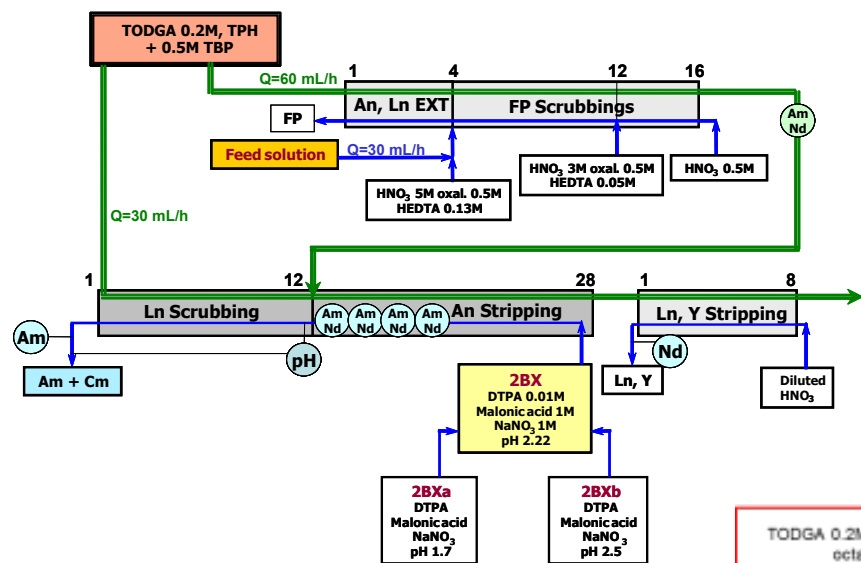
Budget 10,5 M€

Grant 5,55 M€

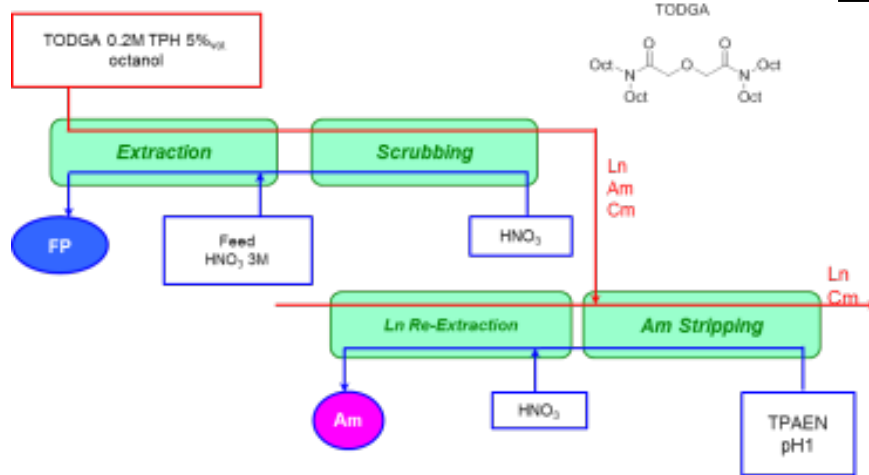
Safety issues



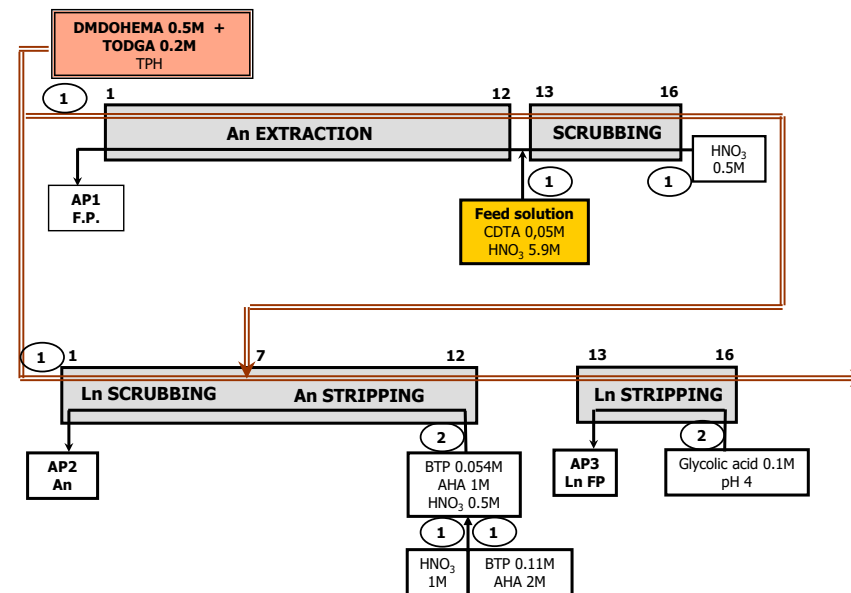




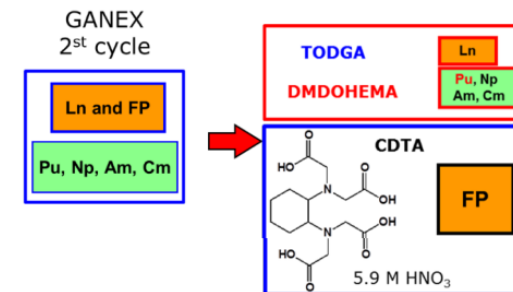
i-SANEX



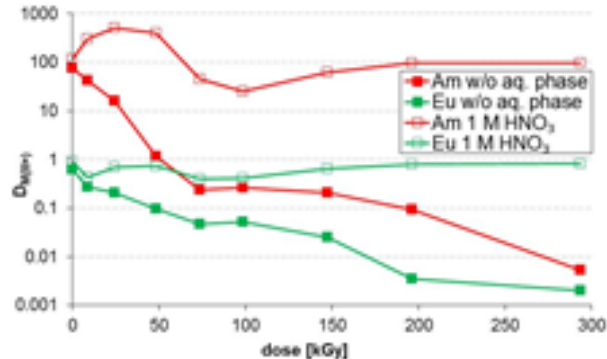
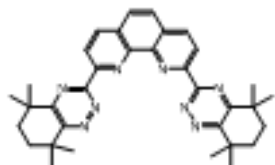
EURO-EXAM



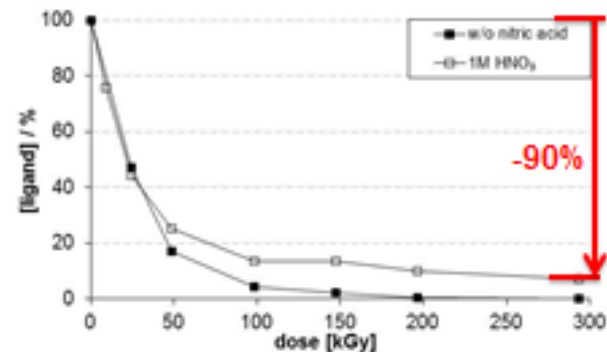
EURO-GANEX



## Liquid-liquid extraction (CyMe<sub>4</sub>BTPPhen) comparison to HPLC-DAD results



Org.: Irrad. 10 mmol/L CyMe<sub>4</sub>BTPPhen in 1-octanol  
Aq.: fresh 1.0 mol/L HNO<sub>3</sub> + <sup>241</sup>Am/<sup>152</sup>Eu tracer



6

- Decreasing D-values with increasing dose
- HPLC-DAD shows destruction of molecule
- Nitric acid while irradiation stabilizes D-values
- 90% reduction of ligand concentration detected by HPLC-DAD  
⇒ due to 1:2 complex, D-value should drop down ~ two orders of magnitude

New built species during radiolysis,  
able to extract An/Ln  
⇒ mass spectroscopy

## Loading capacity of degraded organic GANEX solvent

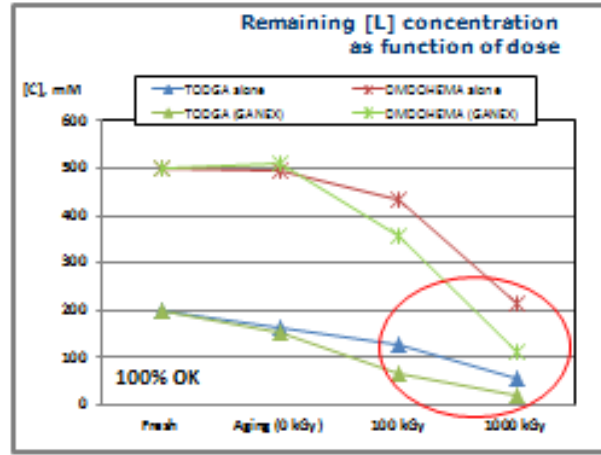
Euro-GANEX



- 0.2 mol/L TODGA
- 0.5 mol/L DMDOHEMA
- In kerosene (OK)

Loading capacity studies are needed!!!

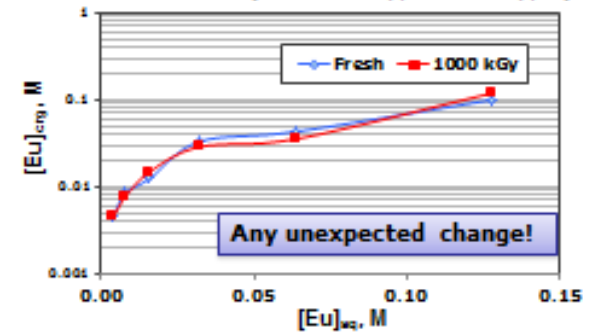
More than 50% degradation of both extracting agents.



20

CIEMAT - 2nd year SACESS Project Meeting, 20-21 April, Warsaw

Ln(III) loading capacity after irradiation (1000 KGy, 1.5 kGy/h).

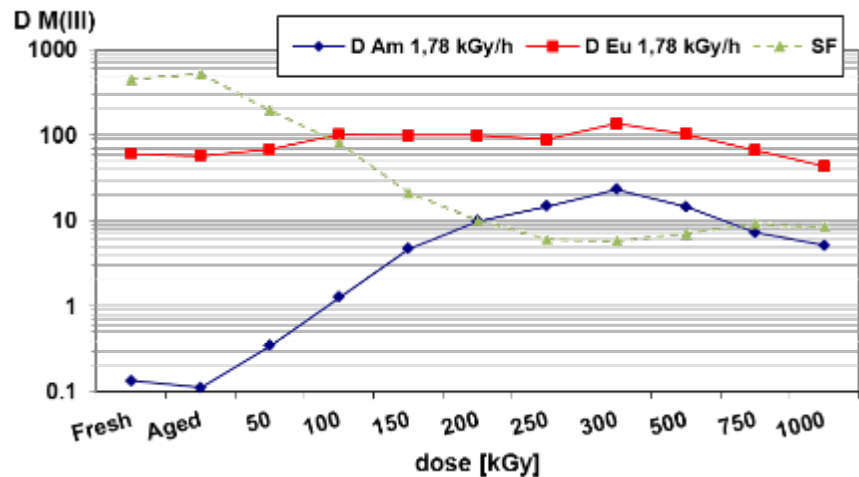


Organic Solution: 0.2 M TODGA + 0.5M DMDOHEMA in OK.  
Aqueous solution: [HNO<sub>3</sub>] = 4 mol/L and Eu(III) concentrations from 0.004 M to 0.128 M, spiked with <sup>152</sup>Eu (1000 Bq/mL).

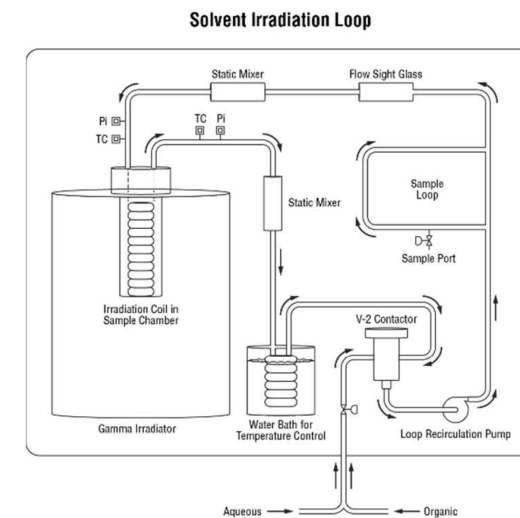
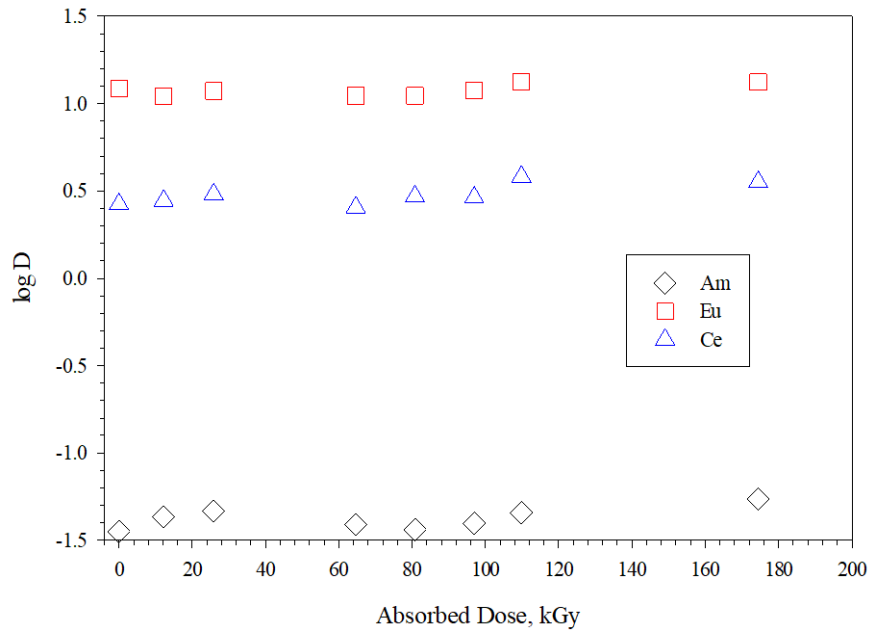
Any unexpected change!



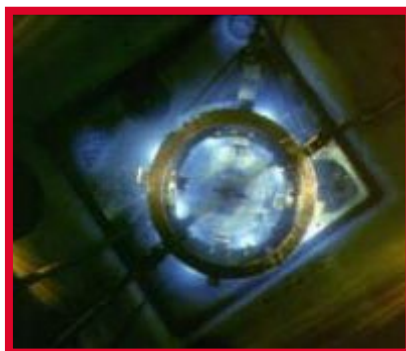
## Static tests



## Dynamic tests



- Closed cap
- Aqueous phase irradiated
- Extraction



- Aerated
- Aqueous & organic phases irradiated in contact





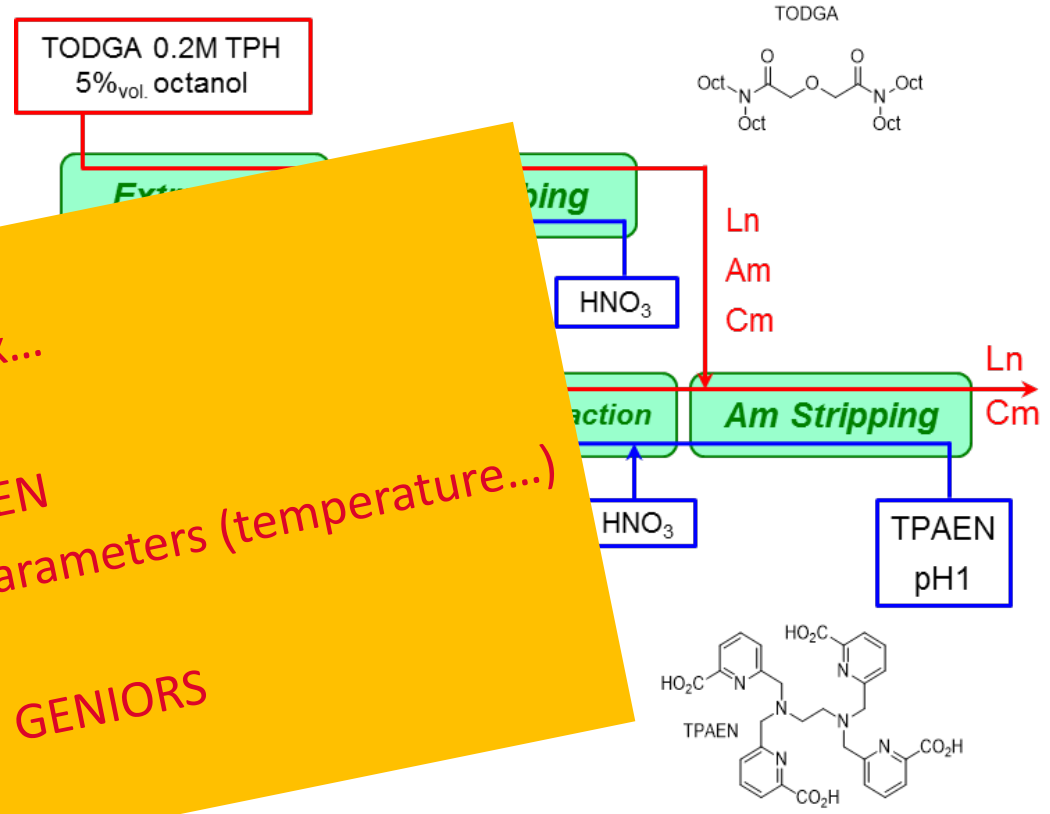
- TODGA + TPAEN → stripping of Am selectively from Cm AND light Ln
- SF(Cm/Am) and (La/Am) ↗ with TPAEN conc.
- TPAEN concentration can be increased up to 2.5 mM
- Am stripping slow but ↗ with temperature
- Light Ln / Am separation with high concentrations of Ln

Solutions:

- 2) Re-evaluate TPAEN concentration
- 3) Temperature

- Experiments with macrocyclic ligands to improve complexation capacity of TPAEN
- Additional data acquisition (Jülich) to develop a thermodynamical model (CEA)
- Spiked test at Jülich in April and June 2016

A lot of issues to fix...  
 Purity of TPAEN  
 Solubility of TPAEN  
 Process maybe too sensitive to some parameters (temperature...)  
 To be improved! → GENIORS



# Electrorefining of irradiated METAPHIX Fuel on aluminium cathode

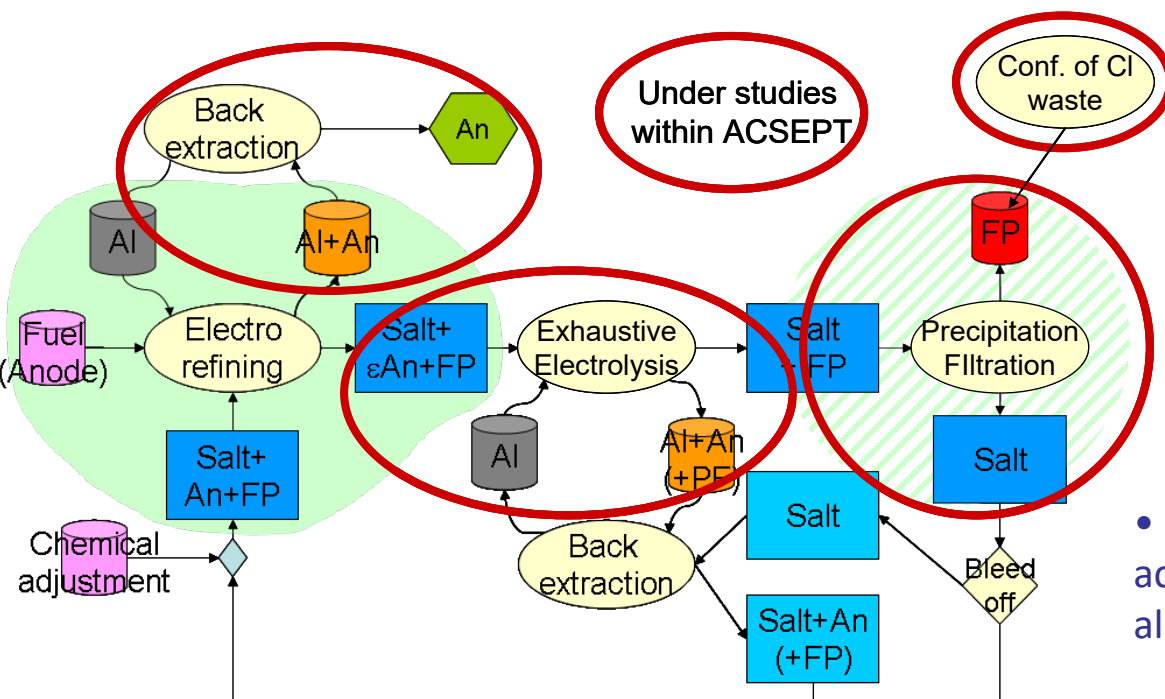


Table 7 Relative content of An and Ln in the deposits from runs 8-11

run	8	9	10	11
U	70.86	80.20	74.08	79.74
Np	1.05	0.75	0.87	0.71
Pu	28.02	18.99	24.97	19.48
Am	0.06	0.05	0.07	0.06
Cm	0.01	0.01	0.01	0.01
sum An	99.99	100.00	99.99	100.00
sum Ln	0.01	0.00	0.01	0.00

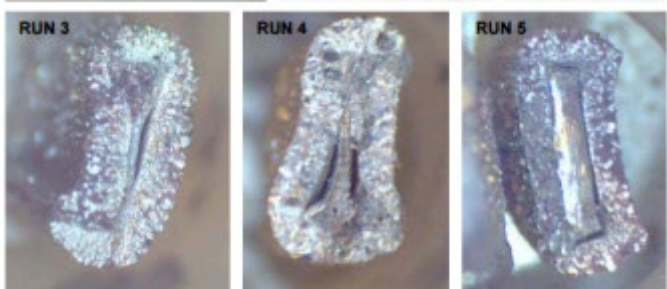
Table 6 Separation factors normalised to U for potentiostatic runs 8-11

run	8	9	10	11
potential	-1.26 V vs. Ag/AgCl			
U	1	1	1	1
Np	2.45	3.85	2.95	3.86
Pu	4.67	7.79	5.30	7.32
Am	17.3	25.3	14.8	20.5
Cm	60.4	83.2	47.3	61.4
La	1879	9294	5109	7432
Ce	3620	6612	4356	6525
Pr	1141	2800	1799	2917
Nd	1820	4008	2152	3610
Pm	1649	3394	1632	2409
Sm	2242	3008	1730	3718
Eu	2427	2903	1495	3623
Gd	2234	2932	1501	2564
Tb	2183	3071	1303	2124
Dy	2572	3191	1666	2104
Y	2145	2641	1666	2610

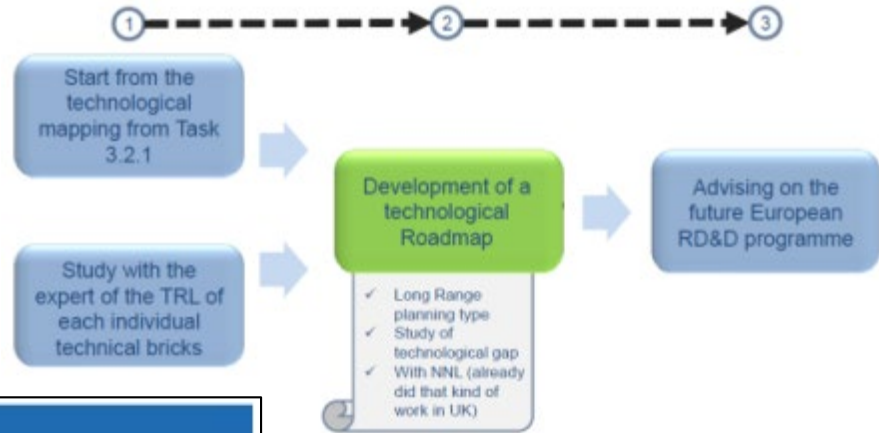


•Based on the IFR concept (USA), the process is centered on the selective electrorefining of solid aluminium cathode in molten chloride

- Quantitative recovery not achievable by electrorefining alone
- exhaustive electrolysis step and salt recycling under study
- Actinide back-extraction from Aluminium is deeply studied



Optical microscopy photographs of the transverse cuts of the Al cathodes after galvanostatic runs 1 - 5



LGI CONSULTING

## ROADMAP Actinide separation processes 2015



Status	4/4	4/6	1/3	3/8	2/6	0/5	0/5	0/1	1/4	0/1	0/1
Steps or studies needed	All step together	All step together	Filter & buffer tank	SO <sub>2</sub> -Ph-BTP DMDOHEMA TOGDA in OK	Pu & mA product Spent solvent 2 <sup>nd</sup> cycle	DEHIBA	DEHIBA	Temperature range of operation	Pu & mA selfheating	Hydrogen generation	Long term effect of solvent on materiel
	U stripping	Ln stripping	Flowsheet equipment	Hydrazine	U product	Hydrazine	Hydrazine		FP selfheating		
	U scrubbing	An stripping 1		Fuel feed	Spent solvent 1 <sup>st</sup> cycle	CDTA	CDTA		Cooling system		
	U extraction	TRU scrubbing	Piping & valves	AHA	Ln product	DMDOHEMA TOGDA in OK	DMDOHEMA TOGDA in OK	U selfheating			
		TRU extract		Nitric acid	FP raffinate	HNO <sub>3</sub> /SO <sub>2</sub> -Ph-BTP/AHA	HNO <sub>3</sub> /SO <sub>2</sub> -Ph-BTP/AHA				
Type of studies or steps	GANEX 1 <sup>st</sup> cycle	GANEX 2 <sup>nd</sup> cycle	Technological needs	Safety and stability studies needed	Radiotoxicity studies needed	Concentration range studies needed	Flow range studies needed	Temperature range studies needed	Thermodynamic behaviour studies needed	Flammability and explosion studies needed	Long term studies needed

EURO-GANEX in a lab (spanning columns 1-3)

EURO-GANEX in a pilot facility (spanning columns 1-12)

Joly, P.; Boo, E. SACSESS roadmap — actinide separation processes; 2015.

[www.sacsess.eu](http://www.sacsess.eu)

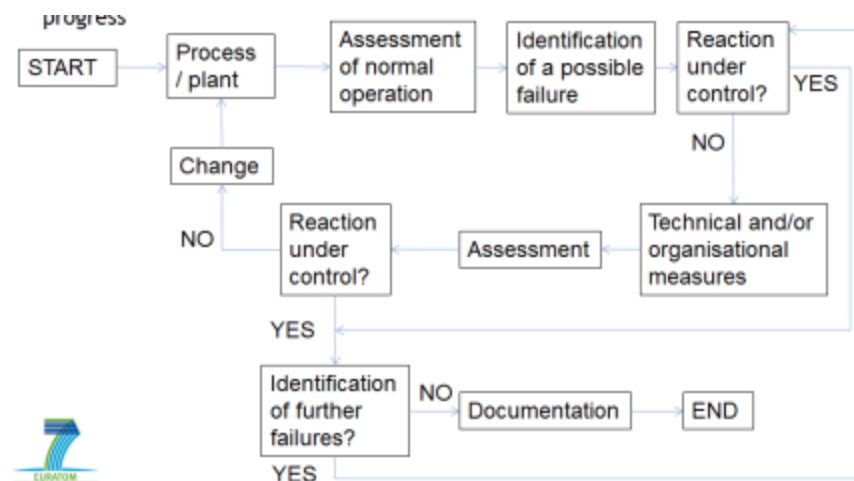


## Global Safety

- Perform safety analyses on hydro and pyro processes to determine weaknesses in their safety and drive experimental programmes of the future to optimise against these issues
- Do this by developing tools that use tools and techniques from the partner nations
- Deploy them with the help of experts in aqueous and pyro reprocessing

The methodology is now established, based on HAZOP approach (April 2014)

Safety case studies were performed in a dedicated workshop (Sept. 2014 & Sept. 2015)





**TURNING  
SPENT NUCLEAR FUEL  
INTO A RESOURCE**

**GENIORS**

**FROM FUEL TO FUEL  
MOX FOR GEN IV**



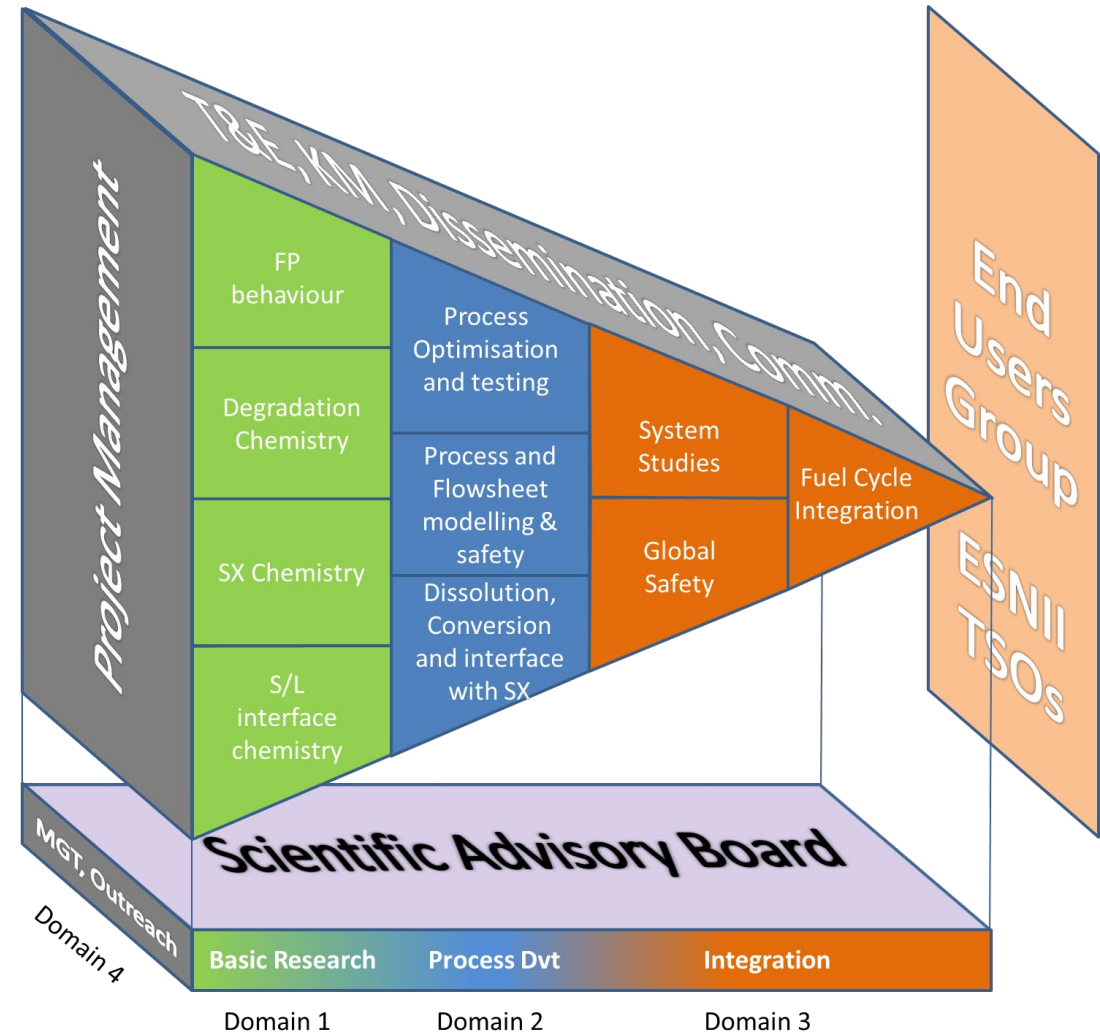
## GEN IV Integrated Oxide fuels recycling strategies

6/2017 – 5/2021

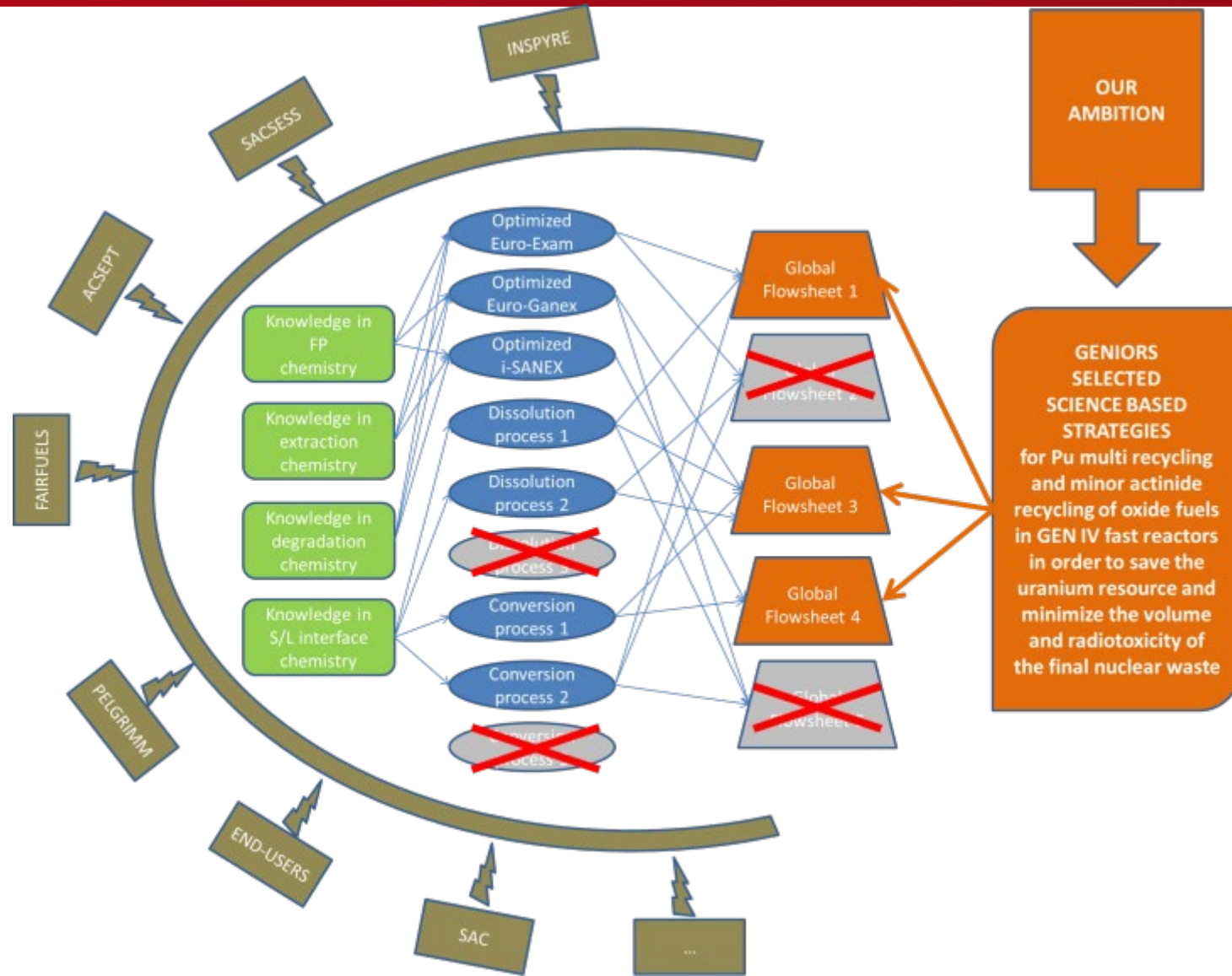
24 Partners, 11 countries

Budget 7,5M€, EU grant 5M€

<b>CEA</b>	<b>JRC-ITU</b>	<b>UEDIN</b>
<b>CHALMERS</b>	<b>JUELICH</b>	<b>UNIMAN</b>
<b>CIEMAT</b>	<b>KIT</b>	<b>UNIPR</b>
<b>CNRS</b>	<b>LGI</b>	<b>ULEEDS</b>
<b>CTU</b>	<b>NNL</b>	<b>UREAD</b>
<b>ICHTJ</b>	<b>POLIMI</b>	<b>ULANC</b>
<b>IIC</b>	<b>SCK-CEN</b>	<b>EDF</b>
<b>IRSN</b>	<b>TWENTE</b>	<b>AREVA</b>



Cooperation agreement with DOE (I-NERI project),



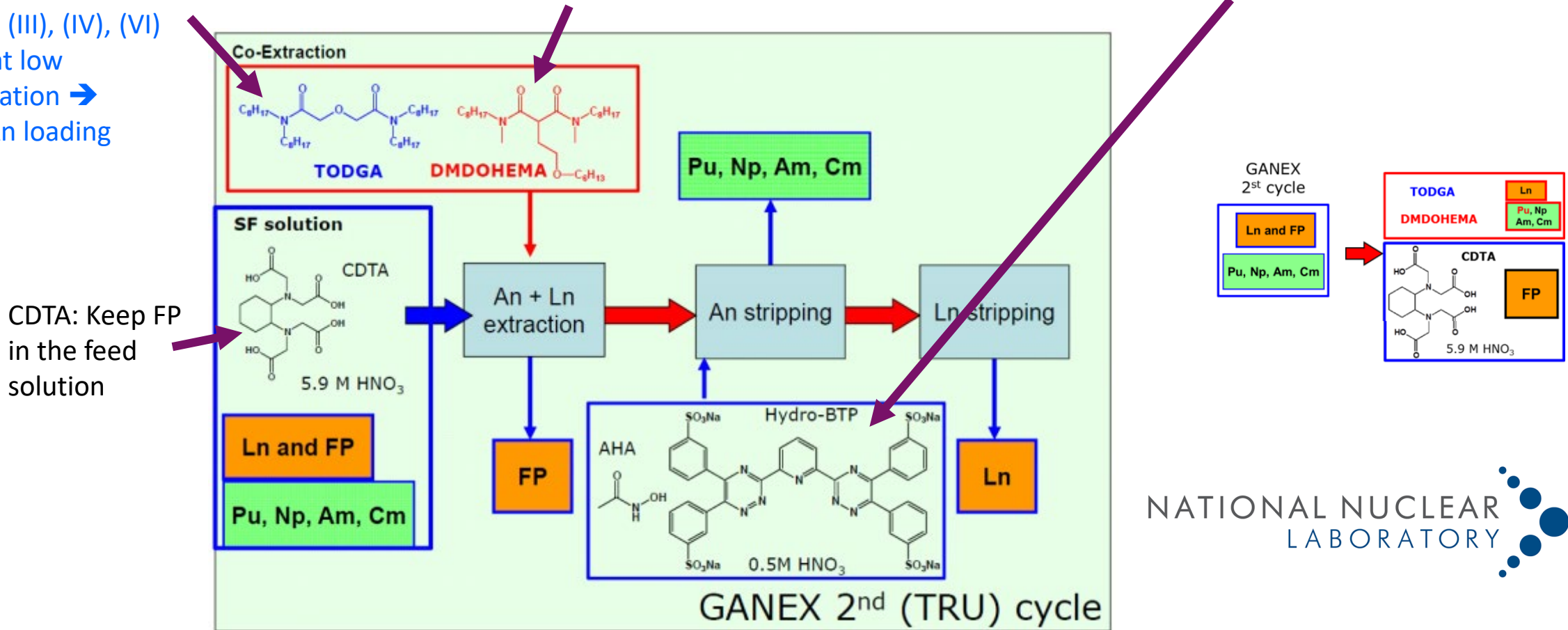




TODGA: Very strong complexation with actinides (III), (IV), (VI)  
→ used at low concentration → limited An loading

DMDOHEMA: Phase modifier to avoid 3rd phase formation by TODGA at high acidity and high loading

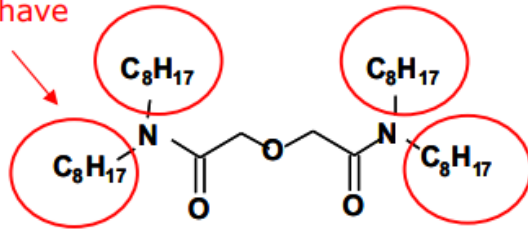
H-BTP: strip selectively the An from the organic phase – potential issues with S at conversion step



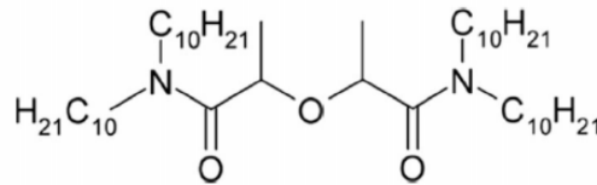


### Increase the loading capacity

Side chains have an impact !!



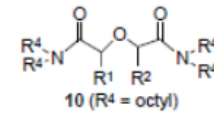
- Increased chain length strongly affects the limiting organic concentration.
- A point is reached where the organic phase seems to be stable – with Nd...
- Chain length (number of C) is limited by the increasing viscosity. Especially at high loadings



**mTDDGA !**

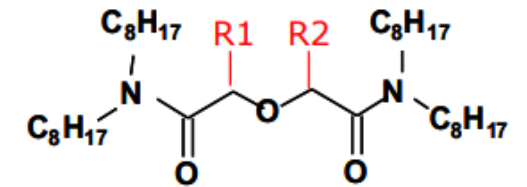
### Decrease the complexation strength

Central groups makes an impact !!



10a = **TWE21**, R1 = Me, R2 = H

10b = **TWE14**, R1 = R2 = Me



- Groups inserted at central carbons exert steric hindrance and thereby affects complexation strength.
- D-values drop orders of magnitude inserting two methyl groups.





Parameter	TODGA-GANEX	mTDDGA-GANEX
<b>Organic formulation</b>	TODGA (0.2M) +DMDOHEMA (0.5M) mixture	Only mTDDGA (0.5M)
<b>Diluents</b>	kerosene	n-dodecane
<b>Pu loading limit</b>	~ 20 g/L	32 g/L
<b>3<sup>rd</sup> phase formation</b>	Yes, at high Pu and acid conc.	No, even at high Pu and acid conc.
<b>Acidity</b>	0.01-3.0 M	0.01-6.0 M
<b>D value for Sr, Mo, Fe</b>	~ 1	~0.1 (10 times lower)

UNIVERSITY OF TWENTE.

**mTDDGA could be a promising candidate for a simplified organic formulation for future EURO-GANEX process.**

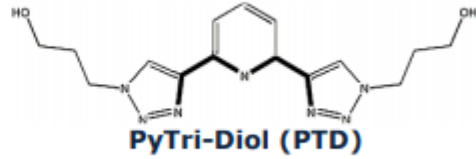




1. An inventory of the description of each loop as well as the current status of operation of each loop
2. An inventory of methods/methodologies of assessing the dose-rate for each loop
3. A definition of a common system to study
4. A common source of extractants, diluents and acids must be identified and used by all the partners involved.
5. A rough flowsheet will be provided by Andreas Geist (simplified flowsheet based on the Juelich process), where he will point-out where there is not sufficient data. This flowsheet is supposed to be adapted to each LOOP and reported on the outcome
6. Each Loop will report if the system can be run in the respective facilities
7. Each loop should report an estimate date for starting the test



**STRIPPING SOLVENT FORMULATION**  
0.08 M PTD in 0.4-0.5 M HNO<sub>3</sub>  
for *i*-SANEX and EURO-GANEX processes



## Process performances

- Experiments with macro-concentrations of <sup>241</sup>Am (1 mM), <sup>152</sup>Eu spike, in presence of 0.02M lanthanides for *i*-SANEX process;
- Experiments with macro-concentrations of <sup>241</sup>Am (1 mM) and <sup>239</sup>Pu (10 mM), <sup>152</sup>Eu spike, in presence of 0.02M lanthanides for EURO-GANEX process;



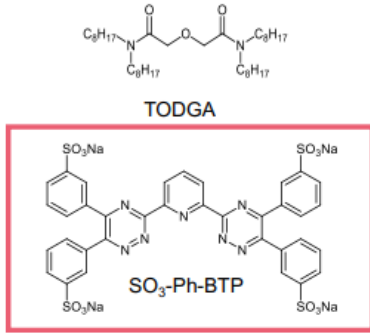
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DI PARMA

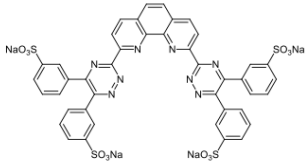
## Radiolytic stability studies

- to go further in the radiochemical stability of PTD-based extracting system to confirm the identity of the observed PTD degradation products
- to study the generation of gaseous products from irradiated TODGA-PTD system

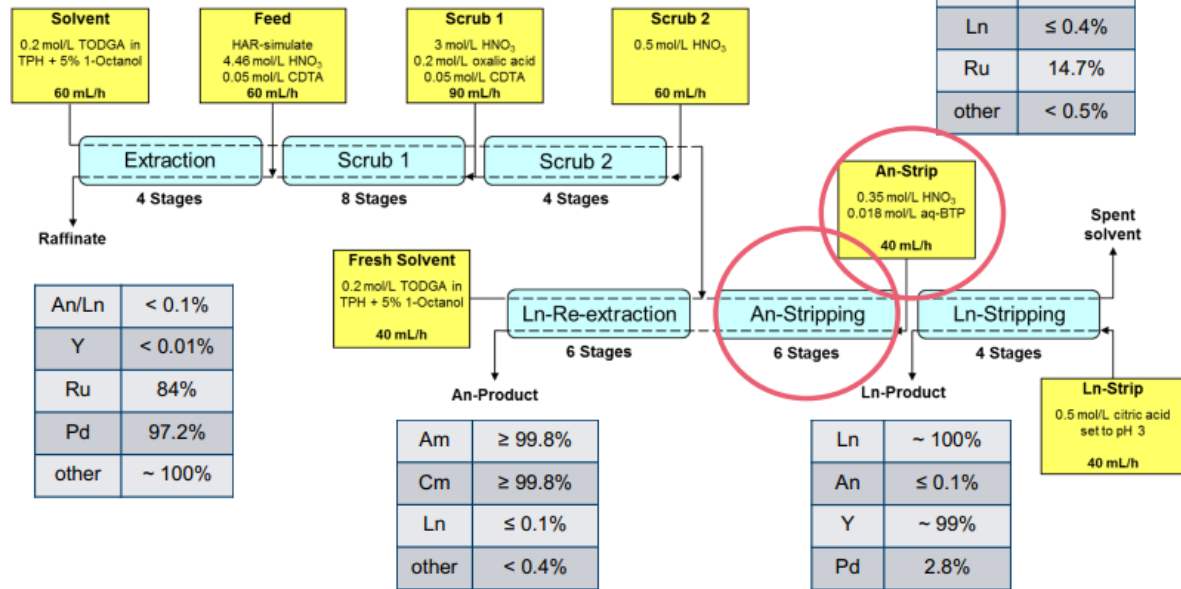


- No hydrodynamic problems or 3<sup>rd</sup> phase formation
- Change An-Strip section to make it Am(III) selective

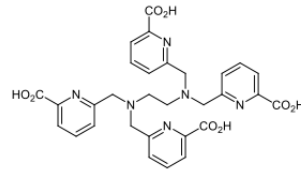
## 1<sup>st</sup> alternative: TS-BTPhen<sup>[1-2]</sup>



- Good Am/Cm selectivity (SF ~ 3.6)
- Good Am/Ln<sub>all</sub> selectivity
- Difficult synthesis
  - not reliable
  - Not reproducible
- Still interested in the ligand, if synthesis works!

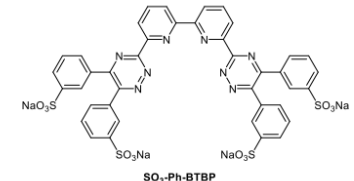


## 2<sup>nd</sup> alternative: H<sub>4</sub>TPAEN<sup>[1-2]</sup>



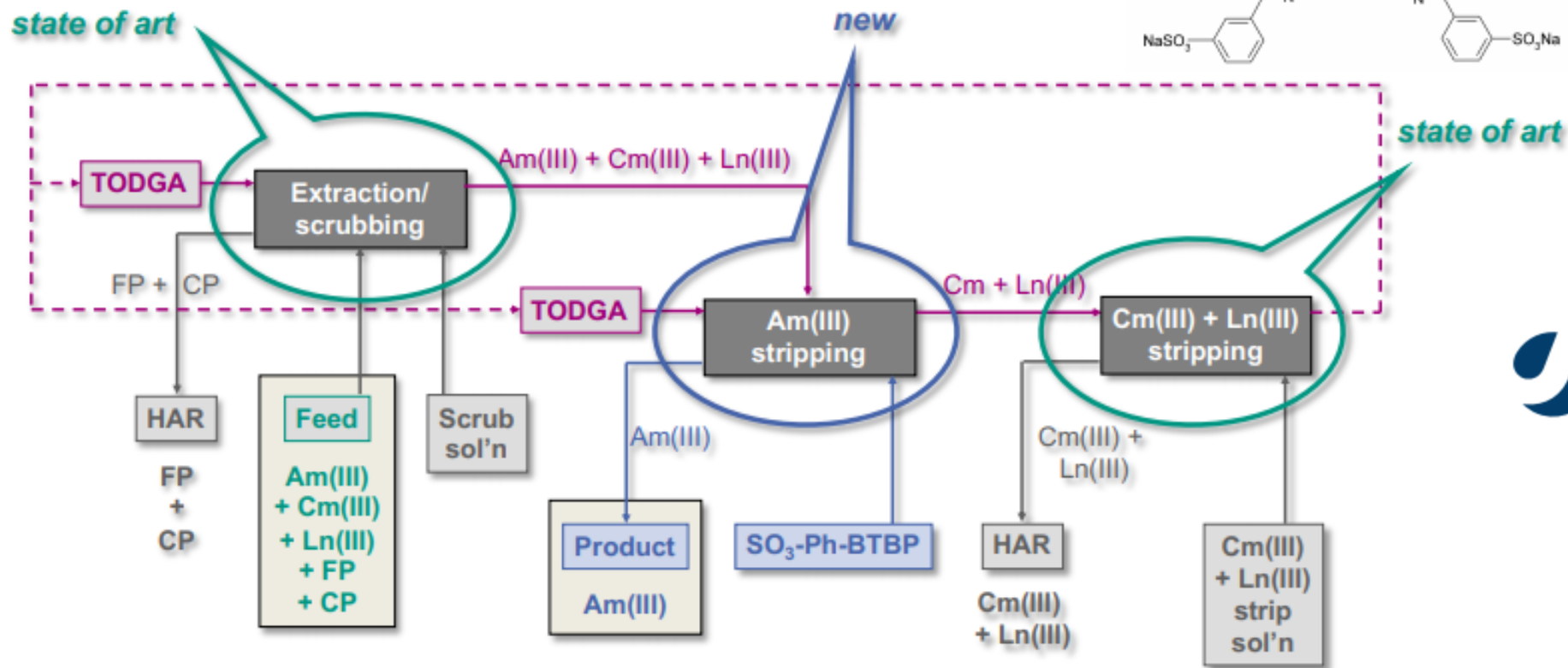
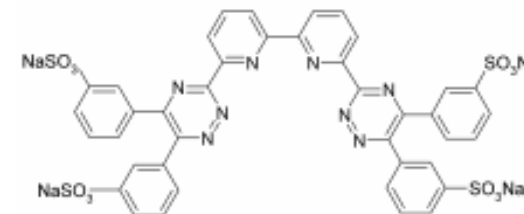
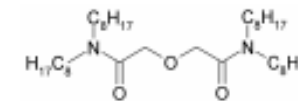
- Good Am/Cm selectivity (SF ~ 4)
- Difficult Am/Ln<sub>all</sub> selectivity (La/Ce)
- Synthesis okay
- Solubility issues (only low concentrations applicable)
- Chosen for process development and demonstration in SACSESS

## 3<sup>rd</sup> alternative: SO<sub>3</sub>-Ph-BTBP,

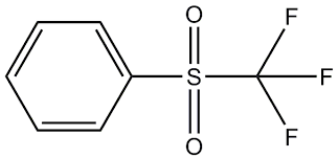
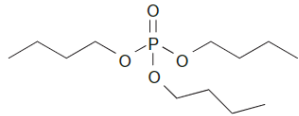
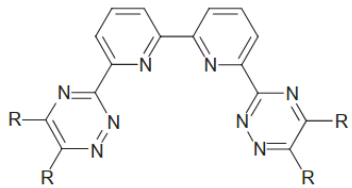
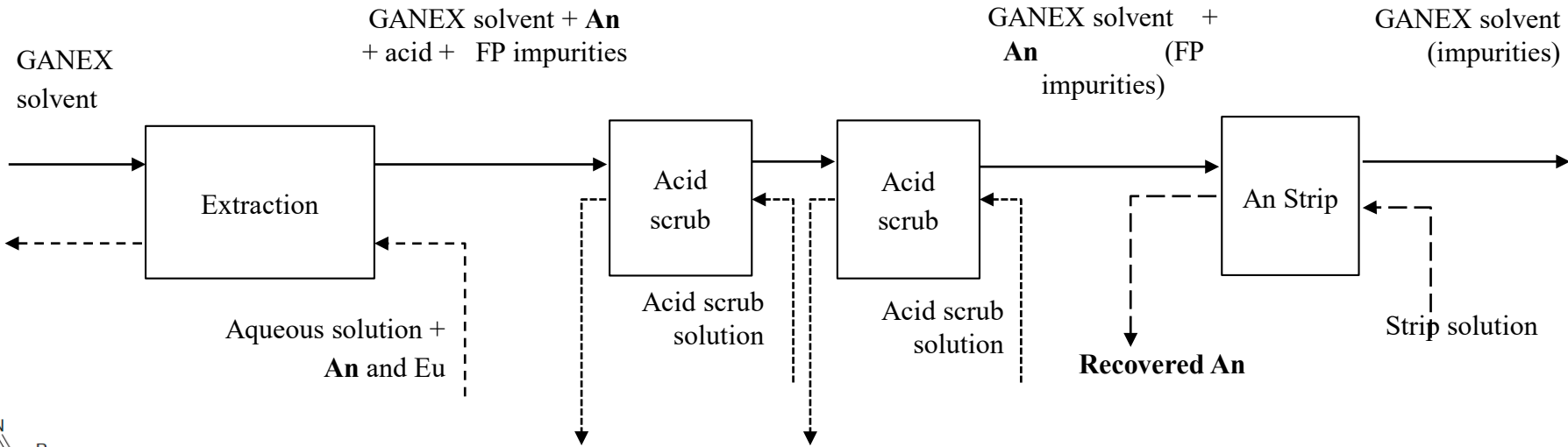


- Medium Am/Cm selectivity (SF ~ 2.5)
- Good Am/Ln<sub>light</sub> selectivity (La-Gd)
- Synthesis okay
- High solubility
- Chosen for further process development and demonstration in GENIORS

- Am(III) stripping section calculations —  $SF_{Cm/Am} \approx 2.6$ 
  - Collaboration with JÜLICH
  - Work in progress



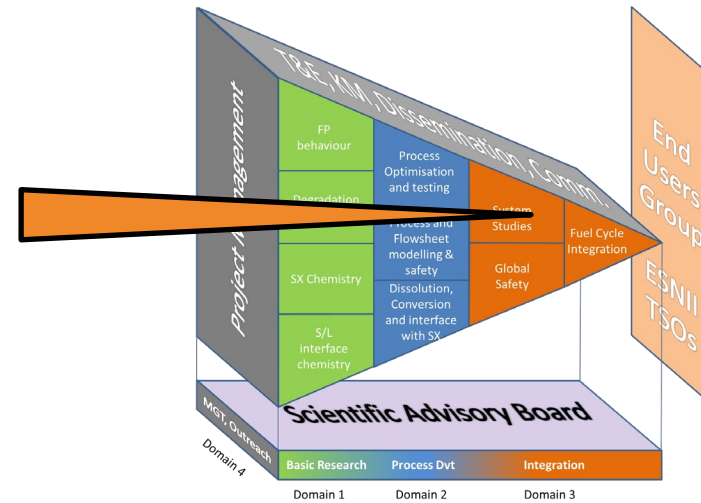
# CHALMEX – a potential simpler GANEX option Batch Process Test (Real Nuclear Waste)







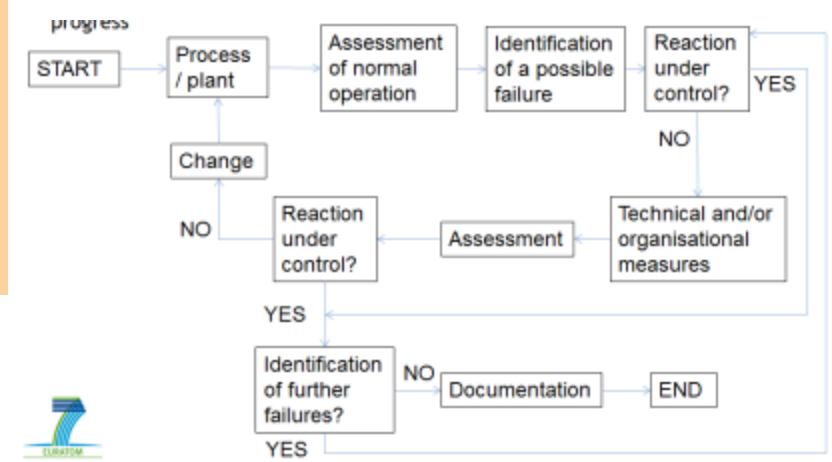
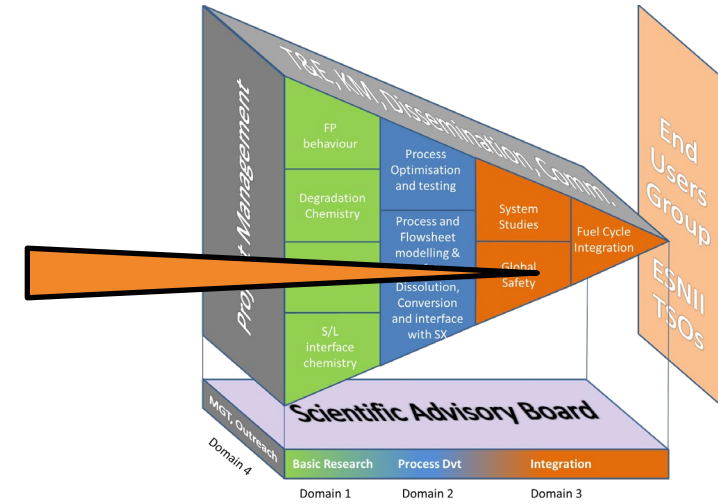
- Developing processes towards industrialisation studies
- Assessing and illustrating the holistic effects on the nuclear fuel cycle that occur from fundamental changes to the chemistry at the heart of its key processes.
- **Concept Design of a Euro-GANEX Plant**
- **Comparing SX processes for heterogeneous recycling**
- **Process Mapping Studies**
- **“Sim-plant” – engineering simulation of integrated plants**
- **Impact Studies**



Status	4/4	4/6	1/3	3/8	2/6	0/5	0/5	0/1	1/4	0/1	0/1	
Steps or studies needed	All step together An stripping 2	Filtr & buffer tank An stripping 1 TRU scrubbing TRU extract	Flow sheet major issue Piping & valves	SO <sub>2</sub> /H <sub>2</sub> O/HTF DMSO/DMF Hydrazine DEHBA in OX Fuel feed AFA N <sub>2</sub> S <sub>2</sub> O <sub>8</sub> acid	Pu & m <sub>235</sub> product Spent solvent 2 <sup>nd</sup> cycle U product U product FP raffinate	DEHBA Hydrazine CDFA CDFA	DEHBA Hydrazine CDFA CDFA	Temperature range of operation Cooling system	Pu & m <sub>235</sub> self-heating FP self-heating Temperature range of operation Thermofluid behaviour studies needed	Hydrogen generation Cooling system	Long term effect of solvent on material Hydrogen generation Thermofluid behaviour studies needed Flammability and explosion studies needed	Long term studies needed
Type of studies or steps	GANEX 1 <sup>st</sup> cycle	GANEX 2 <sup>nd</sup> cycle	Technology needs	Safety and stability studies needed	Radiolysis studies needed	Concentration range studies needed	Flow range studies needed	Temperature range studies needed	Thermofluid behaviour studies needed	Flammability and explosion studies needed	Long term studies needed	
	EURO-GANEX in a lab			EURO-GANEX in a pilot facility								



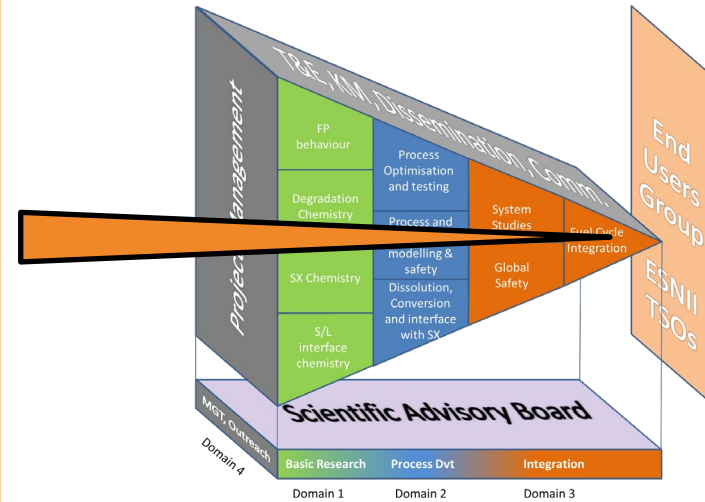
- Developing an emerging process towards industrialisation.
- Studying these requirements for both normal and mal-operations across the fuel cycle
  - Safety Review of a Euro-GANEX plant
  - Hazard Analysis and Criticality Studies
  - Quantification of Corrosions Risks in EURO-GANEX and EXAm Processes





Integrating the work done in GENIORS in a more global approach by creating synergies with other European and international initiatives and by Involving the stakeholders.

- **Clustering with other European projects and international initiatives** – including collaboration with the
- **Stakeholders/end-users Events-** Two dedicated events will be organised gathering the stakeholders potentially interested by the output of GENIORS will be organised at mid-term and at the end of the project.



**Joint workshops with DOE**

DGA extraction chemistry

Diluent issues

**Exchanges with H2020 INSPYRE project on oxide fuel materials**



**TURNING  
SPENT NUCLEAR FUEL  
INTO A RESOURCE**

**TRAINING  
EDUCATION**





## Schools

Uranium, Preston (UK) 7-8 April 2014

Plutonium, Chalmers (SE), 4-8 May 2015

Modelling, Leeds, June 2016?

SACSESS international workshop April 2015

SACSESS international workshop within  
Atalante 2016, June 2016

Student Exchange

Short students presentations

Collaboration with DOE:

Scientific seminars

(Am, kinetics,

Radical Behaviour 2015)



- **A winterschool on industrial fuel fabrication**
- **A winterschool on fuel characterisation and isotopic separation ( $^{15}\text{N}$ )**
- **A summer school on plutonium chemistry together with SACSESS and CINCH**
- **Travel grants for conference participation: 18**
- **Travel and foreign labs training: 4**
- **More than 60 scientific papers**
- **Co-organising an ASGARD session at ATALANTE 2016**
- **Co-organisation of the first ASGARD international workshop at RadChem 2014**
- **Co-organising sessions at TopFuels-2015 together with PELGRIMM project**
- **Several projects in cooperation with the TALISMAN network**





**The Radical Behaviour Workshop, May 2018, Würtzburg**

**Stakeholders event and topical day on P&T, October 2018, Antwerp**

**Think-tank on process safety issues, October 2018, Antwerp**



**TURNING**  
**SPENT NUCLEAR FUEL**  
**INTO A RESOURCE**

THANK YOU

